

In presenting the dissertation as a partial fulfillment of the requirements for an advanced degree from the Georgia Institute of Technology, I agree that the Library of the Institute shall make it available for inspection and circulation in accordance with its regulations governing materials of this type. I agree that permission to copy from, or to publish from, this dissertation may be granted by the professor under whose direction it was written, or, in his absence, by the Dean of the Graduate Division when such copying or publication is solely for scholarly purposes and does not involve potential financial gain. It is understood that any copying from, or publication of, this dissertation which involves potential financial gain will not be allowed without written permission.

3/17/65

b

CALIBRATION AND DATA REDUCTION
OF AN UV SPECTROPHOTOPOLARIMETER

A THESIS

Presented to
The Faculty of the Graduate Division
by
Ellis Bayley Hodgdon

In Partial Fulfillment
of the Requirements for the Degree
Master of Science in Physics

Georgia Institute of Technology
October, 1966

OF AN UV SPECTROPHOTOPOLARIMETER

Chairman

Date approved by Chairman: 10/28/66

ACKNOWLEDGMENTS

The author wishes to thank Dr. Howard Edwards for his valuable assistance and suggestions. Drs. C. D. Cooper and E. Rhodes were also responsible for many comments and suggestions. The author wishes to express his appreciation to his colleagues at the Space Sciences Branch at Georgia Institute of Technology, Mr. Milford Brown of the Balloon Branch at Holloman Air Force Base, New Mexico, and Mr. Cal Skelton of Telecomputing Services, Inc. who helped make the flight possible. Mr. Bill Simpson has helped in the preparation of the diagrams. Mrs. Maria Elena Austin is responsible for the neat execution of the manuscript.

TABLE OF CONTENTS

	Page
ACKNOWLEDGMENTS	ii
LIST OF TABLES	iv
LIST OF ILLUSTRATIONS	v
SUMMARY	vi
Chapter	
I. INTRODUCTION	1
II. INSTRUMENTATION PACKAGE	8
Photomultiplier Tube Signals	
Polarimeter Design and AC Generator Signal	
Polarimeter Construction	
Support Information	
III. OPTICAL CALIBRATION	19
Objective	
Specific Procedure	
IV. DATA REDUCTION	31
General Problems in Data Reduction	
Specific Problems in Data Reduction	
V. SUMMARY AND CONCLUSIONS	47
APPENDIX A	49
APPENDIX B	59
APPENDIX C	64
BIBLIOGRAPHY	136

LIST OF TABLES

Table		Page
1.	Commutator Segments	40

LIST OF ILLUSTRATIONS

Figure		Page
1.	Spectrometer Showing Major Components	3
2.	Gondola Showing Major Components	5
3.	Optical Arrangement of the Ebert-Fastie Spectrometer-Polarimeter	9
4.	Calibration Program Flow Chart	25
5.	Plot of C Versus Wave Length	26
6.	Plot of r_r Versus Wave Length	27
7.	Plot of r_p Versus Wave Length	28
8.	Plot of δ Versus Wave Length	29
9.	General Flow of Information	33
10.	FM Data Converter Flow Chart	35
11.	Commutator Converter Flow Chart	36
12.	Addition of Wave Length Flow Chart	38
13.	Commutator Reduction Flow Chart	41
14.	Main Data Reduction Flow Chart	42
15.	Spectral Intensity of a Portion of the UV Sky	44
16.	Degree of Polarization of a Portion of the UV Sky	45
17.	Spectral Intensity of the UV Sky Radiation	46

SUMMARY

A spectrophotopolarimeter, which is designed to measure the intensity and polarization of skylight radiation at altitudes of greater than 100,000 feet, produces a large volume of data and must be suitably calibrated prior to any measurements. The instrument uses imperfect optical elements, and the effect of these optical components is determined by the calibration procedure. Calibration is simple to perform, but, like the data reduction which follows, requires the use of digital computers. The data reduction involves manipulating the data so that they are in a form to be reduced, and then performing the actual computations.

The spectrophotopolarimeter is a combination of two instruments: one, a spectrometer which uses photomultiplier tubes to measure the wavelength range of 2000 Å to 4000 Å with 16 Å resolution, and the other, a polarimeter which uses a rotating retardation plate followed optically by a linear polarizer. The output of the photomultiplier tubes is a composite AC signal which has a DC component and harmonics of twice and four times the rotational frequency of the retardation plate. By analyzing these components, the polarization and the intensity can be determined. The output of the photomultiplier tubes is digitized at a high rate so that the harmonics can be accurately determined.

Some actual data have been obtained, but their presentation only demonstrates that the calibration procedure and the data reduction procedure are performing satisfactorily. No attempt has been made to reduce the large volume of data that is produced, but only enough to show that the data reduction chain is feasible.

CHAPTER I

INTRODUCTION

A balloon-borne ultraviolet (2000 to 4000 Å) spectrophotopolarimeter, which is designed to measure the intensity and polarization of the natural sky backgrounds at an altitude of 120,000 feet, generates a large volume of data during a typical flight of approximately eight hours. The spectrometer portion of the system is basically an Ebert-Fastie arrangement with a 50 cm. focal length mirror and theoretical f/5 optics.^{1,2} The polarization measurement portion is essentially a Sekera polarimeter,³⁻⁵ which consists of a rotating retardation plate followed optically by a linear polarizer. The light passing through this linear polarizer is measured by a photomultiplier tube. The intensity and polarization parameters can be determined by analysis of the AC components of the signal from the PM tube.

The actual hardware that was flown is described in detail elsewhere,⁶ but a brief description will be repeated so that the flow of information can be followed from the light that strikes the entrance slit of the spectrometer to the actual numbers for intensity and polarization data. Although the mathematics is not complicated, the large amount of data that is produced requires the use of electronic computing equipment. This thesis will give a detailed description of the data handling techniques that have been used on previous flights, including the steps through which the data must pass before the results can be obtained. The instrument and the calibration procedure are unique in that no perfect optical components

are required anywhere, e.g., an imperfect linear polarizer is one that permits some of the unwanted orthogonal component of light to pass through, and an imperfect retardation plate is one which exhibits some additional linear polarization besides retarding the two orthogonal components.

Although some actual data of skylight intensity are presented, the main purpose of this thesis is to show the process by which these data were obtained and the process by which the instrument was calibrated in order to obtain these data. Consideration is always given to the effect of imperfect optical elements and the amount of imperfectness is determined by the calibration procedure.

A general idea of the flight package can be obtained from Figures 1 and 2. These pictures show the spectrometer, yoke and gondola just prior to the 1 July 1965 launch, and important features are as follows.

In Figure 1: The detector head contains all the components necessary to measure the amount of light passing through the exit slit of the spectrometer. The quarter-wave plate and its drive mechanism provides a method of determining the polarization of the incident radiation. The sunshade limits the field of view of the spectrometer and eliminates some reflected light, and the guard cell sensors activate an auxiliary "semi-shutter" which reduces the light entering the spectrometer by approximately two orders of magnitude. The coarse PC (pointing control) sensors provide an error signal to the PC amplifier when the spectrometer is pointing considerably away from the sun, while the fine eye block provides the error signals for fine positioning of the spectrometer system reference axis, which the pointing control attempts to maintain pointed at the sun at all times. The elevation servo provides the torque necessary to point the

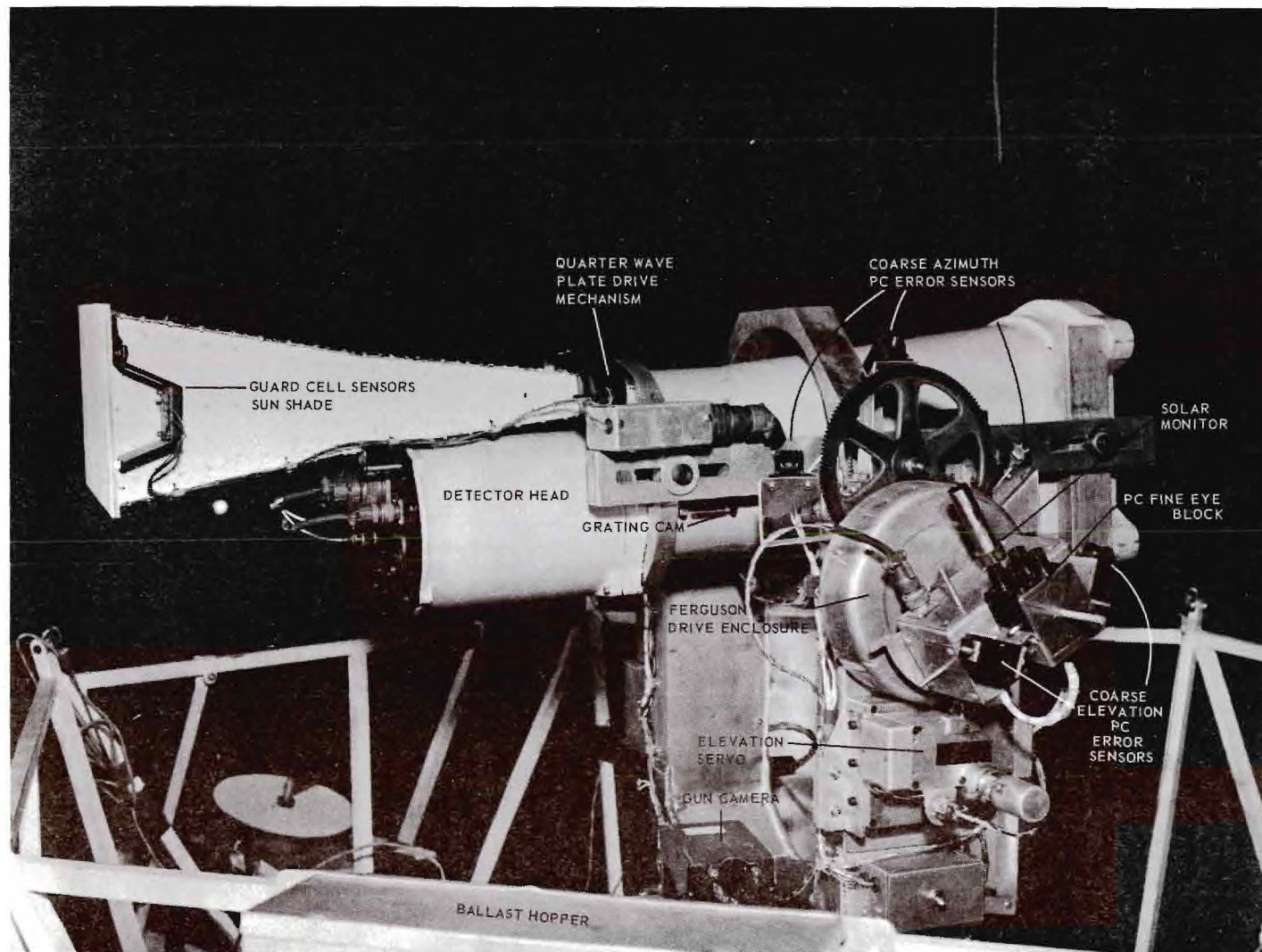


Figure 1. Spectrometer Showing Major Components.

spectrometer system reference axis at the sun. The Ferguson stepping drive imparts an intermittent motion to the spectrometer. Under the influence of this drive the spectrometer is stationary for 30 seconds and moves 15 degrees with respect to the spectrometer system reference axis in the next 30 seconds. The solar monitor provides a means of determining an "on-sun" condition and provides the reference axis from which the spectrometer steps.

In Figure 2: The ballast hoppers, supplied by Air Force Cambridge Research Laboratories (AFCRL), are one means of controlling the ascent rate of the balloon. The yoke assembly holds the spectrometer while the spider supports the yoke and provides some shock protection. The control panel serves as an electrical junction box and provides means of controlling some functions of the flight package and monitoring some of the systems. The gun camera takes a picture of the spectrometer every two minutes through a convex rear view truck mirror to serve as a backup for the pointing control. (If the pointing control were to fail and lock onto something other than the sun, the position of the spectrometer could be determined from the film.) The flight control package, also provided by AFCRL, provides three switch closures by radio command from the ground: drop ballast, telemetry on-off, spectrometer package on-off. The vehicle from which the package was launched can be seen in the background, and some of the equipment used during the pre-flight checkout can be seen on the ground beside the package.

Three actual flights have been made with the basic package, but the first two fell somewhat short of being a total success. The first flight, on 26 August 1964, was aborted shortly after reaching float altitude because of a premature failure of the electronics batteries and stoppage of

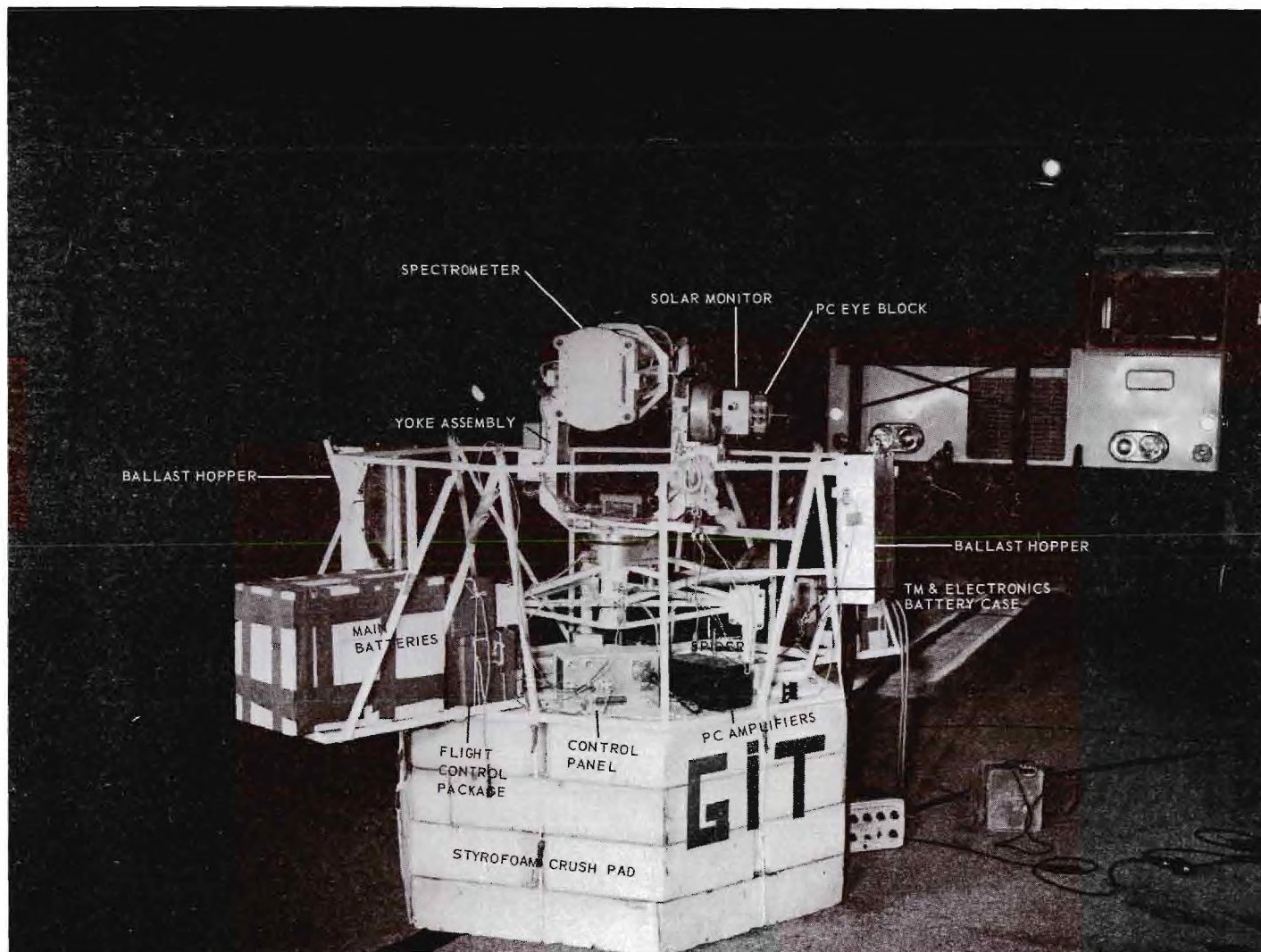


Figure 2. Gondola Showing Major Components.

the quarter-wave plate drive. The pointing control also failed to perform properly. The instrument suffered major damage on impact and the optics of the spectrometer were fouled by transportation over unfavorable terrain back to the launch area.

The second flight, on 1 July 1965, was a trifle more successful. A slight mixup of instructions and drift of the telemetry caused the data not to be received satisfactorily until after the balloon had reached 100,000 feet. A more serious problem developed since the FAA requires that visibility flags be flown every fifty feet when the gondola and the balloon are separated by a long load line. The device which was to deploy these flags singly as the gondola dropped beneath the balloon via the let down reel malfunctioned and deployed all the flags before the gondola had dropped sufficiently. As a result, the flag line became entangled in the spectrometer yoke and prevented the pointing control from operating properly.

From a portion of the data, it was discovered that the spectrometer had randomly found the sun for approximately one hour and forty-five minutes. This time was accumulated mainly after reaching float altitude when the gyrations of the gondola were such as to bring the pointing control and solar monitor around to the sun. It is data recorded at these "on-sun" times which are presented later.

The third flight on 12 July 1966, seemed to be more successful, although sufficient data have not been reduced at the present to ascertain proper operation of all systems. It is known that a wire broke on the elevation scan potentiometer, which gives an indication of the relative angle between the spectrometer and the spectrometer system reference axis,

so that the gun camera data will have to be used to determine the scatter angle of the radiation being measured, but this is not believed to be a serious problem. With each flight the instrumentation package is improved and modified, although the changes are never major and the basic design remains intact.

The brief description of the instrumentation package follows, the flow of information being emphasized. The data reduction techniques and procedures are described in detail, and some limited results from the 1 July 1965 flight are also given.

CHAPTER II

INSTRUMENTATION PACKAGE

Data from several sources must be combined in order to obtain the final results of intensity and state of polarization of the skylight radiation at a given scatter angle from the sun and at a given wave length. To obtain the intensity and polarization of the incident radiation, the signals from the two photomultiplier tubes and the AC generator of the polarimeter must be utilized, while a grating switch signal and the output from the elevation scan potentiometer give the wave length and scatter angle respectively. All the data from the balloon package are telemetered in real time to the ground and recorded on analog tape recorders.

A mathematical description of a polarized light optical system is facilitated by the use of Stokes vectors and Mueller calculus (see Appendix A). A Stokes vector is a four element column vector which completely describes the intensity and state of polarization of radiation, while Mueller calculus uses four by four matrices to describe the effect that optical components have on light. The Stokes vector of the transmitted radiation can be obtained by operating on the Stokes vector of the incident radiation with the proper Mueller matrix for an optical system.

Photomultiplier Tube Signals

The basic optical design of the complete spectrophotopolarimeter is shown in Figure 3. Light entering the entrance slit S_1 strikes the spherical mirror M and is collimated toward the grating G where it is refracted according to the wave length relation for Ebert geometry:

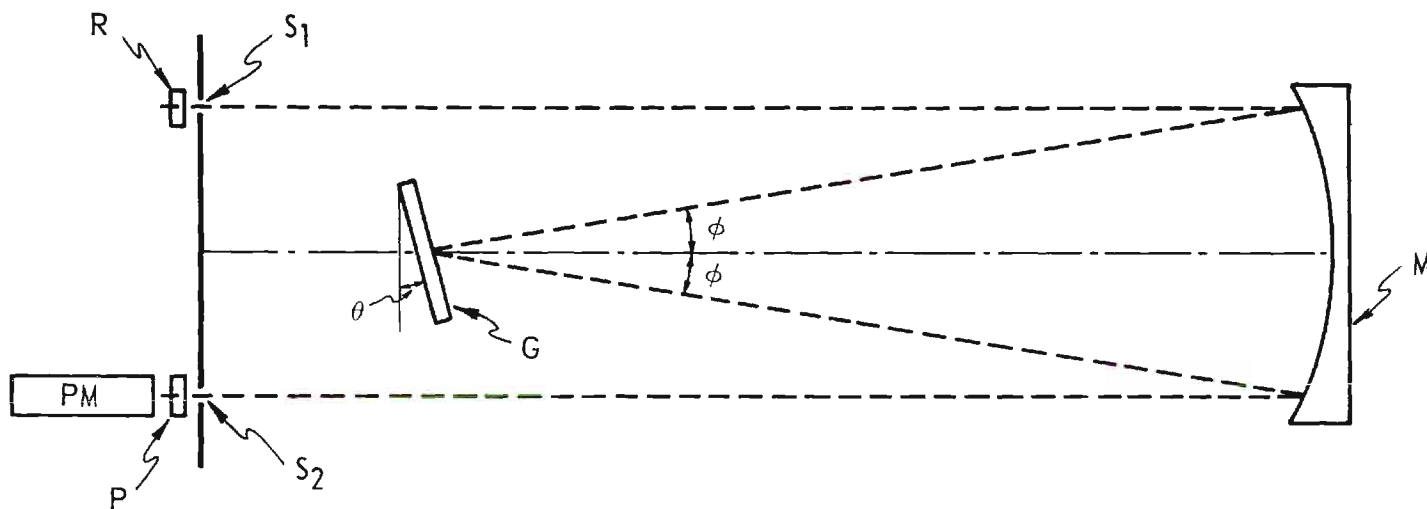


Figure 3. Optical Arrangement of the Ebert-Fastie Spectrometer-Polarimeter.

$$n\lambda = 2 d \cos \Phi \cos \theta \quad , \quad (1)$$

where n is the spectral order, λ is the wave length that appears at the exit slit S_2 , Φ is the angle between the axis of symmetry and the light incident upon the grating, and θ is the angle of rotation between the grating normal and the axis of the instrument. The diffracted light of wave length λ , after leaving the grating, strikes the mirror and is refocused on the exit slit, through which it passes and is detected and measured by the photomultiplier tube PM. The retardation plate R and the linear polarizer P are components of the polarimeter and will be described later.

The grating is driven by a cam and cam follower mechanical arrangement. The cam is driven by a governed 3 RPM DC motor and is cut so that a linear relation exists between the rotational angle θ and the wave length λ which appears at the exit slit. The cam is cut by the manufacturer of the basic Ebert-Fastie spectrometer for a particular grating ruling (in this case, 2160 grooves/mm.) and the wave length range to be covered.

Two photomultiplier tubes are used to cover the 2000 to 4000 Å range. One is a "solar blind" tube used primarily below 3100 Å while the other is used in conjunction with a Corning #7-54 filter for a 2800 to 4000 Å band pass. Figure 5 shows a calibration parameter, C , which is a measure of the spectral sensitivity of the entire system, including the spectral response of the photomultiplier tubes. Each photomultiplier tube signal is amplified by a high impedance nonlinear amplifier which has a dynamic range of approximately four log cycles. The output of these amplifiers is 0 to 5 volts, which is the input requirements for the telemetry system.

The photomultiplier tubes, amplifiers, and the associated subsystems are contained in a pressurized detector head mounted on the slit end of

of the spectrometer (see Figure 1). The detector head contains a DC-DC converter which supplies high voltage (up to 3000 volts) for the photomultiplier tubes and a regulated center-tapped power supply which supplies power for the amplifiers and the DC-DC converter. Since the nonlinear characteristic of the PM tube amplifiers is temperature sensitive, the amplifiers are contained in a temperature controlled ($+ 85^{\circ}\text{F} \pm 3^{\circ}\text{F}$) oven for stability. A small calibration light source, which provides an input light to the PM tubes during the calibration cycle to obtain a nominal calibration point, and its current regulated power supply are also contained in the detector head as well as monitoring and calibration circuitry. The airtight construction of the detector head is such that it will maintain a nominal one atmosphere pressure even at float altitude so that the high voltage present will not arc.

Polarimeter Design and AC Generator Signal

Mathematical Description of Polarimeter

Since polarization is present in most spectrometers which employ a grating as a diffracting element, some method of analyzing the polarization of the incident light was decided upon over elimination of the polarization sensitivity of the spectrometer. A Sekera-type polarimeter was constructed and attached to the instrument, and the mathematics evolving from the use of retardation plates and linear polarizers such as in this polarimeter need some explanation. This polarimeter requires a linear polarizer as part of the optical train, but since no polarizer could be found that would transmit sufficiently below 2300 \AA , the spectrometer grating itself, which is an imperfect polarizer, was used for the linear polarizer for the 2000 to 3200 \AA tube.

By placing an imperfect retardation plate of retardance δ , not necessarily precisely $\lambda/4$, in front of a fixed imperfect linear polarizer (in this case, the entire spectrometer system and the polarizer), the intensity and the other Stokes parameters can be found from a partial inverse solution of

$$[A] = [P_o] [R_\beta] [I] , \quad (2)$$

where $[A]$ is the Stokes vector of the light leaving the linear polarizer, $[I]$ is the Stokes vector of the incident radiation, and $[P_o]$ and $[R_\beta]$ are defined by equations (A-17) and (A-28), respectively.

The photomultiplier signal is proportional to the intensity of light striking the photocathode, which can be placed in the following form:

$$I_A = a_1 + a_2 \sin 2\beta + a_3 \cos 2\beta + a_4 \sin 4\beta + a_5 \cos 4\beta \quad (3)$$

where the a 's are Fourier coefficients that have a definite form which is shown in Appendix B and where β is the angle the fast axis of the retarder makes with a reference axis. After the components a_1 , a_2 , a_3 , a_4 , and a_5 are determined by some method of harmonic analysis, the unknown quantities, the modified Stokes parameters of the incident light, I , P , V , and ϕ , are given by

$$I = \frac{1}{C(1 + r_p^2)(1 + r_r^2)} \left[a_1 - \frac{(1 + r_r^2 + 2r_r \cos \delta)}{(1 + r_r^2 - 2r_r \cos \delta)} a_5 \right] \quad (4)$$

$$P = \frac{2(a_4^2 + a_5^2)^{\frac{1}{2}}}{CI(1 - r_p^2)(1 + r_r^2 - 2r_r \cos \delta)} \quad (5)$$

$$V = \frac{a_2 - CI \left(1 + r_p^2\right) \left(1 - r_r^2\right) P \sin 2\phi}{2CI r_r \left(1 - r_p^2 \sin \delta\right)} \quad (6)$$

$$\phi = \frac{1}{2} \tan^{-1} \left(\frac{a_4}{a_5} \right) \quad (7)$$

The parameters C , r_r , r_p , and δ are characteristics of the system and are determined by the calibration procedure. Equations (4) through (7) will therefore determine the modified Stokes parameters of the incident light from the Fourier components of the exit intensity as a function of β .

The parameter δ is the retardance of the phase plate, r_p is the ratio of the minor axis transmission to the major axis transmission for the linear polarizer (ideally, $r_p = 0$), r_r is the ratio of the slow axis transmission to the fast axis transmission for the retarder (ideally, $r_r = 1.0$), and C is the spectral sensitivity of the system.

Initially, the spectrometer was assumed to be only a linear polarizer. However, a comparison of equations (A-17) and (A-25) reveals that the two Mueller matrices for an imperfect linear polarizer and an imperfect retardation plate are similar. Since the intensity is the only quantity measured by the photomultiplier tubes and since the spectrometer is last in the optical train, only the first row of the Mueller matrix which represents the spectrometer is needed. The first row of both the linear polarizer matrix and the retardation plate matrix are identical in form so the spectrometer could be considered to be either an imperfect linear polarizer or an imperfect retardation plate and the results would be the same. This means that the spectrometer could have elliptically polarizing elements, e.g., metallic reflectors, and the results to be derived would be the same as the case of the spectrometer exhibiting only linear polarization.

Effect of Imperfect Optical Elements

Since it was known beforehand that the optical components used were not perfect, it was necessary to determine the effect of such imperfect elements in the optical train. The main component to consider is the linear polarizer, since it is not nearly as perfect as the Glan-Thompson prism used by Sekera. Also, since the spectrometer covered a wide wave length region, a dependence on wave length of the various physical parameters may be considered an imperfection and must be considered. The relationships expressed in equations (9) through (12) form the basis for determining the effect of imperfect optical elements on the determination of the Stokes parameters.

It can be seen that if r_p is known with a fair degree of accuracy and is not unity, then all the polarization parameters can be uniquely determined. If r_p were unity, i.e. no polarizer, then although P , V , and ϕ could not be determined, I could be measured if I were the only quantity of interest, and the requirement for a polarimeter would vanish. While P is proportional to $1/(1 - r_p^2)$, V is essentially proportional to $1/(1 - r_p^2)^2$, so any error in the determination of r_p will have some effect on P , but it would have a greater effect upon the measurement of V .

Other imperfect optical elements will have an effect on the determination of the Stokes vector of the incident light. Investigating the effect of the retardance of the phase plate on the Stokes parameters, we find that if $\delta = 0$ or 180° , then although V could not be determined, I , P , and ϕ could. As expected, $\delta = 90^\circ$ leads to no difficulty in any determination. The other extreme on the phase plate would be if $r_r = 0$, which would correspond to the phase plate being a perfect linear polarizer. If

this were the case, then again V could not be determined, but I , P , and ϕ could be.

In general, the requirements placed on the optical elements in the train would be that in the wave length region of interest $r_p < 1$, $r_r > 0$, $0^\circ < \delta < 180^\circ$, and obviously, $C > 0$. If these conditions are satisfied, then the four modified Stokes parameters (and consequently, the Stokes parameters themselves) of the incident light can be uniquely determined. However, even with these conditions fulfilled and all optical components properly calibrated, thermionic emission in the photomultiplier tube and other sources of noise in the system may seriously affect the measurements if, for example, r_p were close to unity. Therefore, the practical limit on the magnitudes of r_p , r_r , δ , and C which can be tolerated is set by experimental conditions.

It is known that C shows a strong wave length dependence since it includes, among other things, the spectral response of the photomultiplier tube, δ will exhibit a medium wave length dependence, and r_r and r_p will have some slight wave length dependence. The spectrophotopolarimeter would have to be calibrated at as many wave lengths as possible in order to observe these wave length dependencies and also to judge a reasonable confidence level which can be placed on the results.

Polarimeter Construction

The polarimeter which was actually used consisted of two separate systems, one for each photomultiplier tube, each using nominally one-half of the exit and entrance slits. The two retardation plates (R in Figure 3) were rotated at 20 RPS by a governed 4800 RPM DC motor through a 4:1 gear reduction. An AC generator was driven through a 2:1 gear reduction from

the same motor. In principle, if the peak amplitude of the generator output were known, then the arc sine of the ratio of the amplitude at a given time to the peak amplitudes would give the angle of the generator shaft with respect to some reference axis at that time. This angle would then be equal within some constant phase angle to twice the angle of the retardation plate. It can be seen from equation (3) that multiples of the angle of the retardation plate are needed to perform the required harmonic analysis. The output of the AC generator is then fed into the telemetry system.

The linear polarizer (P in Figure 3) for the longer wave length tube is a Polacoat coated quartz disc mounted inside the detector head and aligned so that its axis is along the axis of maximum polarization of the spectrometer. For the shorter wave length tube, since no suitable polarizer could be obtained that would transmit below 2300 \AA and since the instrument is a fair polarizer in the 2000 \AA to 3000 \AA , the instrument itself is used as the linear polarizer and no polarizer is used in the detector head.

Support Information

Two additional pieces of information which relay wave length and scatter angle are needed to complete the minimum information necessary for data reduction. Other information such as temperature, pointing control error signals, and battery voltages are transmitted, although they are not directly involved in the data reduction. Information of a slowly varying nature such as temperature, scatter angle, battery voltages, and error signals are combined by a commutator into one telemetry channel. The wave length data are transmitted on a separate channel.

A ratchet type cam is physically attached to the cam which rotates

the grating. This ratchet cam is unevenly cut so that a microswitch which is activated by the cam is turned on and off at irregular times during one rotation of the cam, but the cycle is repeatable between rotations. For the 1 July 1965 flight, the points at which the grating switch was turned off corresponded to 2086, 2595, 3264, 3774, and 3900 Å. Thus it is possible to find the minimum time interval (and therefore the minimum wave length interval—in this case 126 Å) between consecutive pulses and set the last time of the interval in this case to 3900 Å, and from that point determine the wave length at any time during the forward sweep of the grating. The assumption is made that the grating cam is cut so that a linear relationship exists between the transmitted wave length and the angle of rotation, and a secondary assumption is made that the governed DC motor which drives the grating cam rotates at a constant speed for one rotation. It was felt that a switch closure and opening provided greater resolution than other means such as a potentiometer.

A precision potentiometer is mounted so that its resistance is a measure of the angle between the spectrometer system reference axis, which is, in operation, the line from the instrument to the sun, and the spectrometer axis. A suitable voltage divider provides an output between 1.0 and 5.0 volts (input voltage requirements for the commutator). This potentiometer is calibrated upon final assembly of the spectrometer since the sprocketed drive chain is disconnected when the instrument is shipped.

The other data that are transmitted via the commutator are adjusted by suitable means so that the voltage range is 1.0 and 5.0 volts. These data are commutated along with the scatter angle data (elevation scan potentiometer) onto one telemetry channel. Thus telemetry requirements are

for four channels for continuous data—two PM tubes, the AC generator, and grating switch—and one channel for commutated data.

CHAPTER III

OPTICAL CALIBRATION

Objective

Since quantitative data were required to measure the skylight intensity, the optical system of the instrument had to be calibrated in terms of watts per cm^2 volt out. One method for such a calibration is to measure the characteristics of each component in the optical train and then figure the combined characteristic from the individual ones. However, for expediency and simplicity, a method was devised that permitted the optical calibration of the spectrophotopolarimeter in a maximum of two steps at each wave length of interest. It is possible with this method actually to calibrate the system in one step, if one knows the quantitative amount of light passing through an auxiliary polarizer. There is one serious disadvantage to this method, and that is the quantity of data that is required for calibration. Hand reduction of these data is practically impossible from the time standpoint, and therefore, the computational procedures have to be programmed for the computer. Another problem arises, however, namely the generation of the data in a form that is usable by the computer, but this problem has been essentially solved, and a means has been obtained of reducing the large volume of calibration data. An analog-to-digital converter (ADC) at Telecomputing Services, Inc. uses the analog tape which is generated by the calibration procedures and produces a digital tape in IBM 7094 format which can be used on the Georgia Tech computer. Thus, the entire problem of data handling is essentially alleviated by computer and computing machinery.

The basic problem of calibration can be broken into three categories: (1) the calibration of the quarter-wave plate as to retardance, transmission, and linear polarization, (2) the calibration of the spectrometer for transmission and linear polarization, and (3) the calibration of the photomultiplier tubes for spectral response. The third problem is best solved by means of an NBS Standard of Spectral Irradiance⁷ for which NBS has calibrated the light output versus wave length. It is assumed, however, that transmission losses in the optical train can be accounted for by modification of the spectral response of the photomultiplier tubes. Thus, the spectral response of the whole system which the calibration procedure produces is quite likely to differ from the spectral response furnished by the manufacturer.

For all the different calibrations except the quantitative value of light input versus voltage output, the procedure is fairly simple. A suitable light source (a GE quartz-iodine lamp was used) is placed behind a linear polarizer that can be rotated in fixed increments. The light from this polarizer is then allowed to fall on the entrance slit of the spectrophotopolarimeter. The output is then recorded by some means, either through telemetry onto magnetic tape recorders or by oscillographs from which the data is obtained by ADC or hand reduction, respectively. The angle of polarized light is stepped in its fixed increments until an angle of at least 180° has been passed. For a given wave length, the output is first broken down into components of the frequency of the rotating quarter-wave plate frequency and its harmonics, and then these components undergo a Fourier analysis with the angle of incident polarization as a basis. The system has the distinctly advantageous property that no optical component

(quarter-wave plate, linear polarizers, etc.) has to be perfect because the system allows for imperfections in these devices and actually computes the amount of imperfection.

The calibration for the quantitative value requires only the NBS standard of spectral irradiance which is placed before the entrance slit. The output of the photomultiplier tube is analyzed into components of the rotating quarter-wave plate frequency, and the value of the transmission coefficient, C , for the entire system is calculated.

Specific Procedure

An accessory was constructed that was capable of rotating a linear polarizer in convenient fixed increments of 11.25 degrees. The polarizer was made from a sheet of Polaroid HNB. For the first part of the calibration procedure, this accessory was placed between the light source, a GE quartz-iodine lamp, and the entrance slit of the spectrophotopolarimeter. The polarizer was then rotated by manually pushing a switch at a time which corresponded to the return sweep of the grating. Thus, the polarizer was rotated every twenty seconds, which means that throughout the calibration run, for every sweep of the grating through the wave length region, there was a different angle of polarization of incident light.

For the second part of the calibration procedure, the NBS standard of spectral irradiance was placed a known distance (61.2 cm) from the entrance aperture of the spectrophotopolarimeter. Although this is not the distance at which the lamp was calibrated, it is reported that the inverse square law is valid at distances over 43 cms. Several wave length scans were made with the standard lamp as the light source to serve for calibration purposes.

The calibration procedure is definitely computer oriented. A large volume of data is accumulated, and some of the calculations, although they could be calculated using a desk calculator, are best left for the digital computer. For the utilization of the digital computer, a method of multiple linear regression was used which minimizes a function, G , of the form:

$$G = \sum_{i=1}^N \left[y_i - a_1 - a_2 x_{1i} - a_3 x_{2i} - a_4 x_{3i} - a_5 x_{4i} \right]^2 \quad (8)$$

by adjusting the a 's where, in this case, y_i is the photomultiplier tube output corrected for dark current, $x_{1i} = \sin 2\beta_i$, $x_{2i} = \cos 2\beta_i$, $x_{3i} = \sin 4\beta_i$, and $x_{4i} = \cos 4\beta_i$, where β_i corresponds to the β in equation 3 and the i^{th} value of y .

During a normal computation, a minimum of 25 samples are used in the determination of the a 's; the number of samples is a function of the wavelength interval for which the computation is made. At the present limit of analog-to-digital conversion, 500 samples per second per channel, approximately five samples are obtained as the grating sweeps through 1 Å. Since the resolution of the spectrometer is approximately 16 Å, the intensity is assumed to remain constant during a sweep of 5 Å (25 samples), and no correction is attempted for an intensity change during the sampling time.

The Fourier coefficients [the a 's in equation (8)] are not obtained via a sine or cosine integration, but rather are obtained by a curve fitting process. A test was made to determine if higher order components of β were present, and the higher order coefficients were reduced in magnitude by a factor of 50 or higher. Also, a frequency spectrum analysis was per-

formed on the photomultiplier signal, and similar results were obtained, i.e., only a DC, 2β , and 4β components were measurably present.

The results derived in Appendix B show that the calibration parameters-- r_r , r_p , C, and δ (equations (4) to (7))--can be determined from

$$r_r = \sqrt{\frac{1-k}{1+k}} \quad (9)$$

$$\cos \delta = \frac{d_2 - d_6}{d_2 + d_6} \left(\frac{1 + r_r^2}{2r_r} \right) \quad (10)$$

$$r_p = \sqrt{\frac{kd_1 - d_5}{kd_1 + d_5}} \quad (11)$$

$$CI = \frac{d_1(1+k)}{2(1+r_p^2)}, \quad (12)$$

where

$$k = \sqrt{\frac{d_4 d_5}{d_1(d_2 + d_6)}} \quad (13)$$

and where the d's are defined in Appendix B.

If the total intensity of light falling on the entrance aperture after passing through the polarizer is known, then C can be determined from equation (12). However, if the quantitative value of light passing through the polarizer is not known and a separate determination is needed to determine C, then after performing the required harmonic analysis on the PM tube signal, C can be found from

$$C = \frac{1}{I(1+r_p^2)(1+r_r^2)} \left[a_1 - \frac{1+r_r^2+2r_r \cos \delta}{1+r_r^2-2r_r \cos \delta} a_5 \right] \quad (14)$$

If the source is completely unpolarized, then $P = 0$, and consequently, $a_5 = 0$. With the lamp used, a_5 was approximately three orders of magnitude small than a_1 .

Calibration is complete after the determination of C , whether it comes from equation (12) or (14). No "perfect" optical components, except perhaps for an unpolarized light source, are used, and the calibration could be performed in just one operation. Individual components are not calibrated as such, rather the entire spectrophotopolarimeter is calibrated as a basic unit.

The basic computer program for the calibration procedure is shown in Appendix C while the flow diagram for this program is shown in Figure 4. The calibration data undergoes the same preparation as the regular data, i.e., the input tape has all data digitized, i.e., two photomultiplier tubes and the output of the AC generator, and the wave length calculated for the forward sweep of the grating. No wave length computation is attempted during the return sweep of the grating.

The results of the calibration program are used as input to a multiple linear regression library program which provides a mathematical approximation to the actual wave length dependence of the calibration parameters by fitting the calibration parameter to a specified function of wave length. This regression merely smoothes the data, removes bad calibration points and provides a convenient method of evaluating the calibration parameters. The coefficients which are thus determined are used in the main data reduction program. The calibration curves for C , r_r , r_p , and δ for the 1 July 1965 flight are reproduced in Figures 5, 6, 7, and 8 respectively.

The various coefficients in equations (4) through (7) [for example,

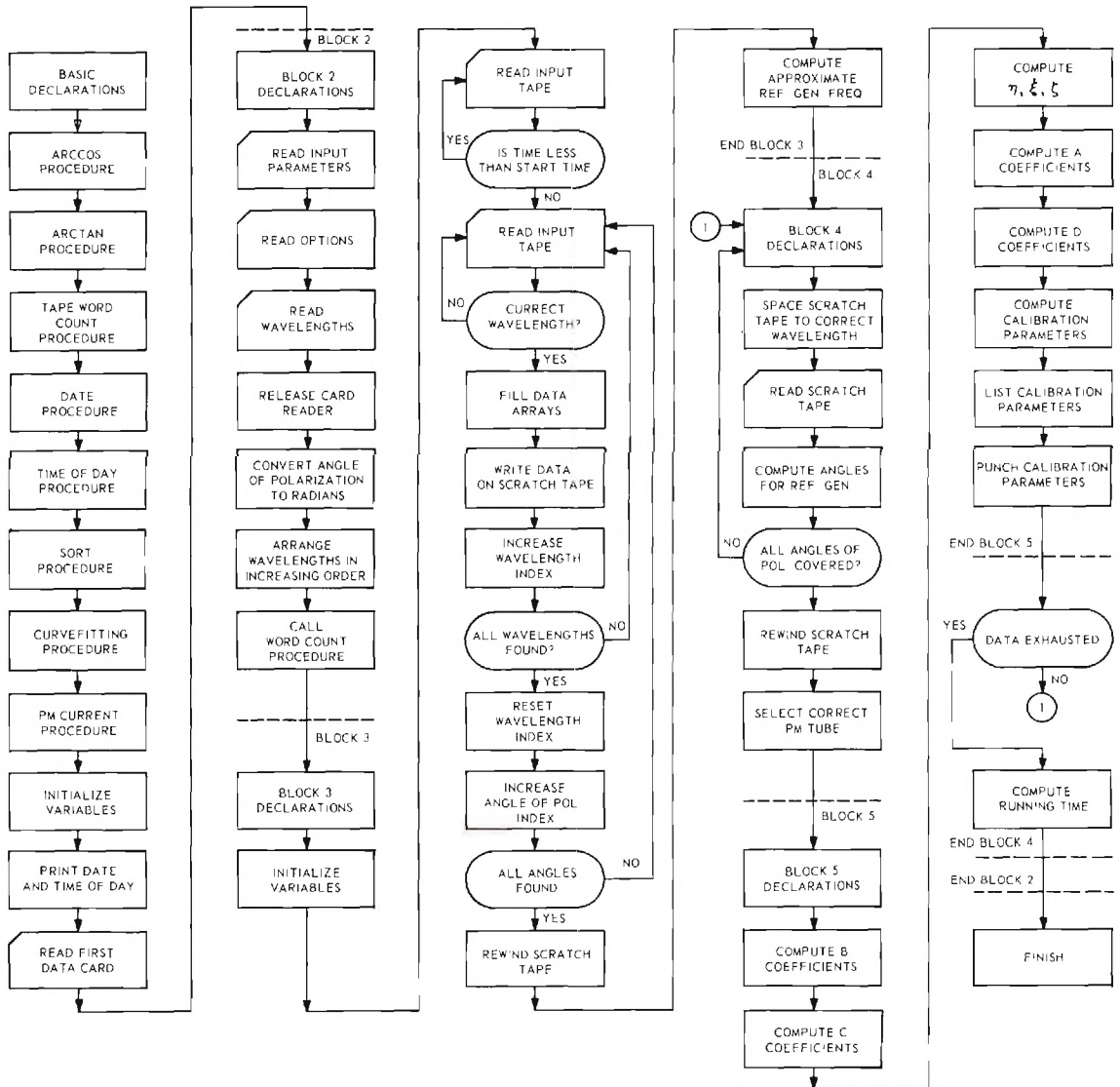


Figure 4. Calibration Program Flow Chart.

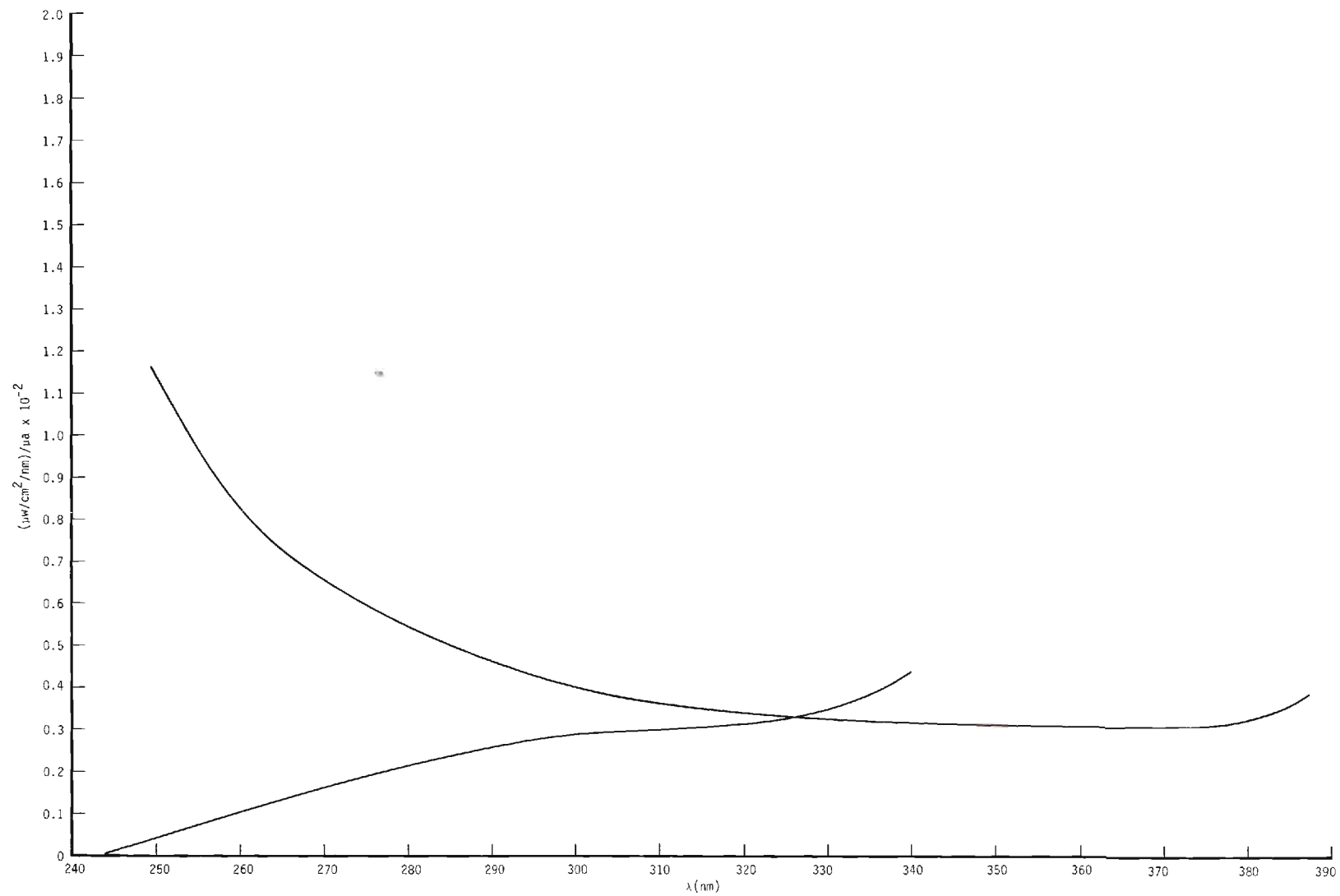


Figure 5. Plot of C Versus Wave Length.

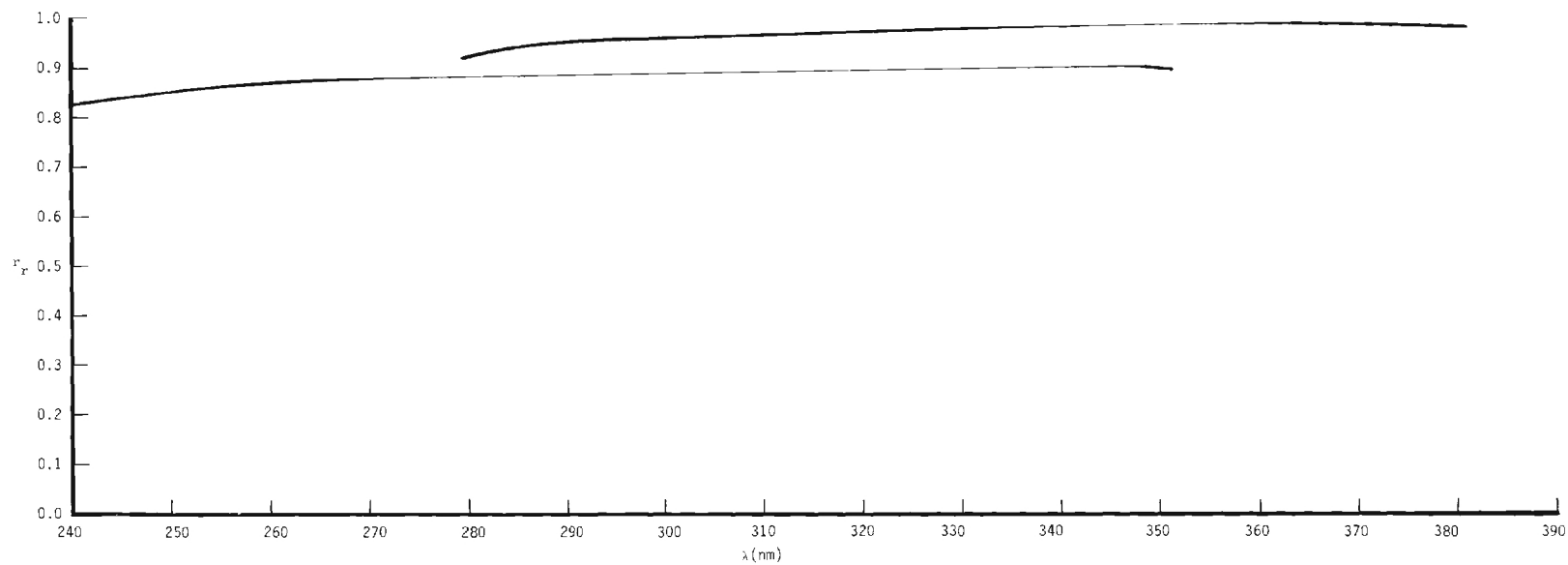


Figure 6. Plot of r_r Versus Wave Length.

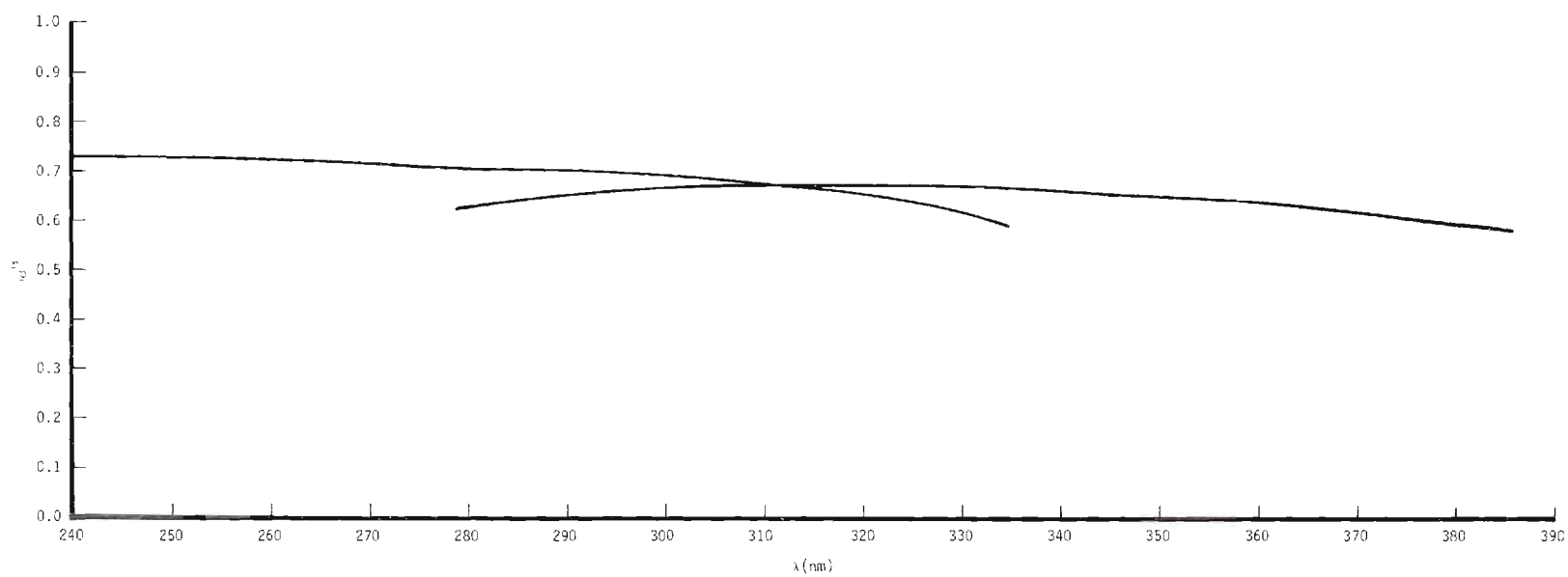


Figure 7. Plot of r_p Versus Wave Length.

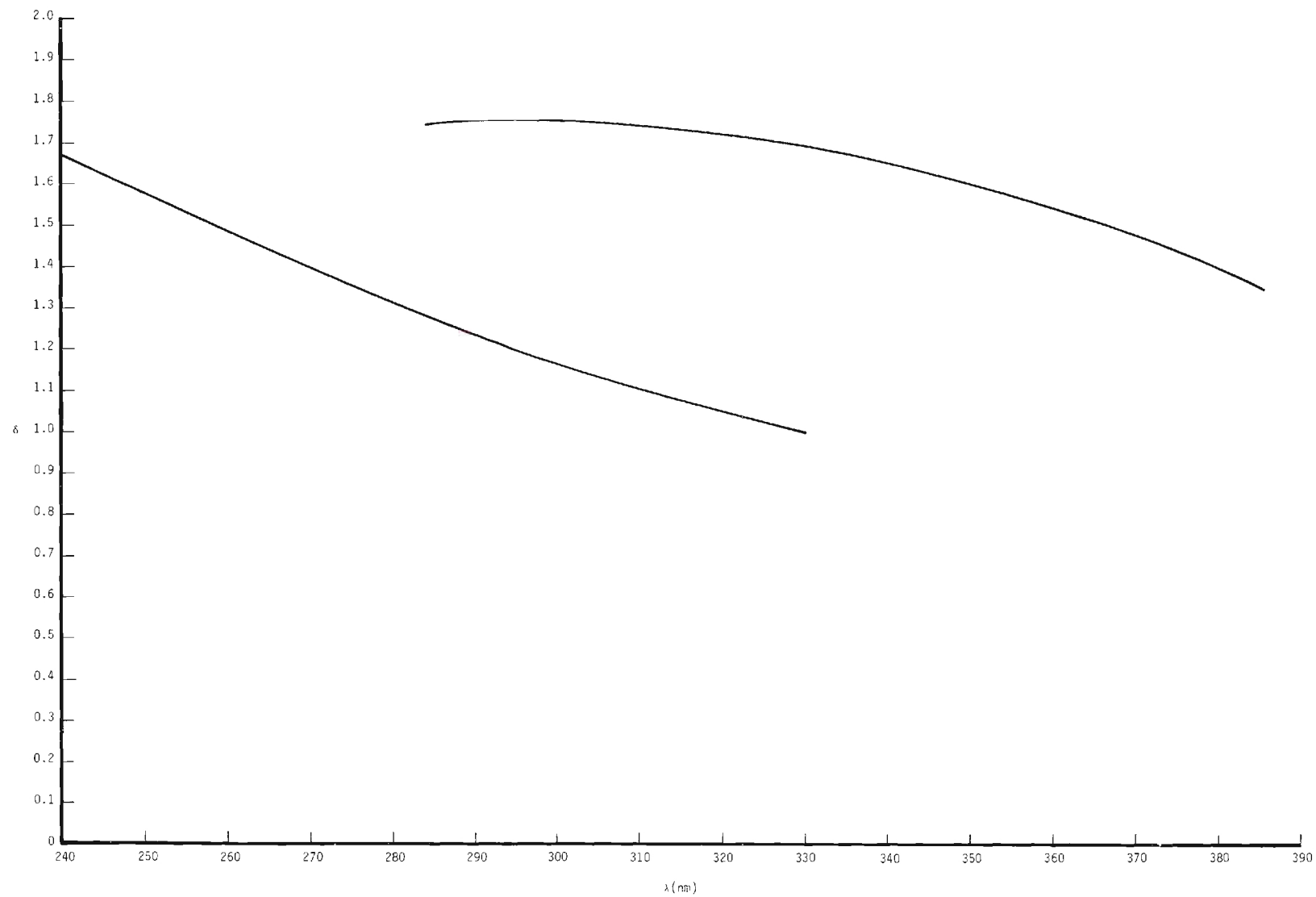


Figure 8. Plot of δ Versus Wave Length.

the coefficients $1/C(1 + r_p^2)(1 + r_r^2)$ in equation (4)] are calculated for various wave lengths and stored on an auxiliary input tape for the main reduction program. Thus the calibration parameters can be changed without having to change the main reduction program. Other data which are included on this input tape are scatter angle and altitude-time profile. After this auxiliary input tape is generated, the main portion of the data reduction can commence.

CHAPTER IV

DATA REDUCTION

Upon termination of the balloon flight, the data which have been recorded on analog tape recorders are processed through analog-to-digital converters (ADC). Since it is necessary to approximate the 40 cps AC generator signal during the computational process, the continuous data (FM data) is sampled at a rate of 500 samples per second per channel. The ADC processes are a service supplied with the balloon launch facilities, and therefore the digital tapes that are received are in a usable but not ideal condition to be used with computing equipment at Georgia Tech. The sampling limitation on the ADC is a total of 1000 samples per second. Therefore two tapes are produced for the four input channels—two photomultiplier tube signals, a grating position indicator, and the AC generator. The commutator data are digitized at a rate of one digital output value for each segment during a frame; with the commutator that was used, this rate was 70 samples per second. A commutator is a switching device that selects sequentially one of a number of inputs and connects it to the output; the commutator that was used had 28 inputs, and it sampled each of these input $2\frac{1}{2}$ times per second. A frame is one string of the 28 samples plus synchronization, and a segment is one input signal during a frame. These tapes produced by ADC are written in a packed 36 bit word which is incompatible with the 48 bit word used by the Georgia Tech Burroughs computer. Therefore a word length conversion is necessary.

A block diagram of the flow of information from the balloon package to the final results is shown in Figure 9. The calibration tapes are made a few days prior to the flight, using telemetry and under all practical conditions of a flight. Thus, the calibration includes any nonlinearity, frequency response and phase shift that might be present in the telemetry system. The altitude and temperature profiles are provided by the launch organization after the completion of the flight, and the altitude profile must be manually fed into the computer program so that the altitude at which the data are obtained can be printed with the data. As a consequence of the wide use of electronic data processing equipment, the amount of data which is handled manually is nominal.

The computer programs which perform these various stages are written in Algol-60 with the programming concept that they should be more general than specific in their application, i.e. if a foreseeable change is made, this should not necessitate any major change in the program.

General Problems in Data Reduction

Every digital tape that is received from the ADC process must first undergo a word length conversion to make the tapes compatible with the Georgia Tech computer. Besides changing the word length from 36 to 48 bits, the converter program also provides an output of the converted data on a labeled tape to facilitate future handling. Two converter programs are used: one, the commutator converter program, converts the single commutator tape and produces an output tape in a similar format as the input tape, and the other, the FM data conversion program, converts and merges the two FM data input tapes into a single output tape. A third program is necessary to add wave length to the FM data output tape. The format

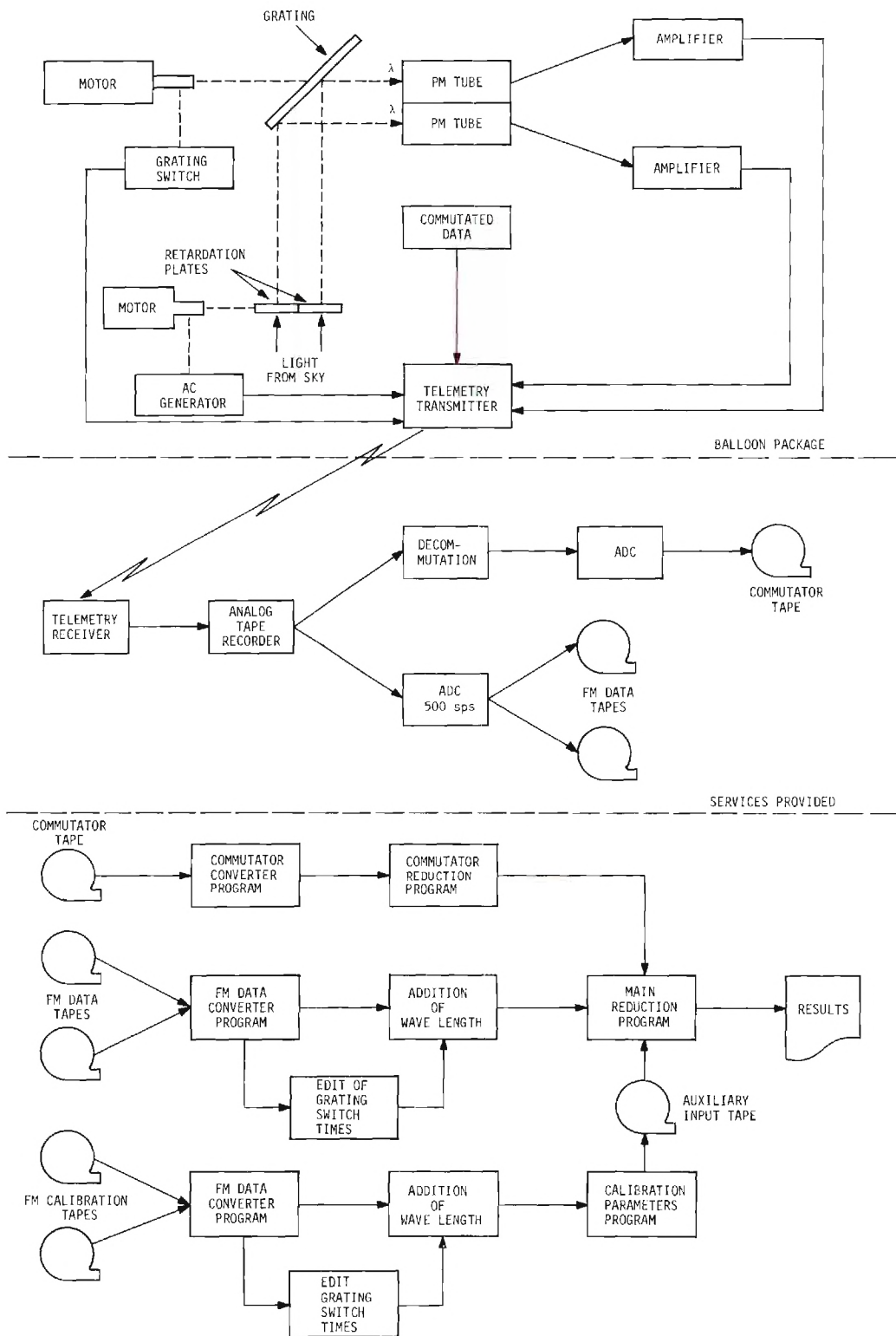


Figure 9. General Flow of Information.

for these tapes is given in Appendix C as well as a detailed explanation of the programs.

These three programs are as follows:

FM Data Converter Program

Basically this program converts the 36 bit digital tape into a digital tape which is usable on the Georgia Tech's Burroughs B-5500 computer. The tapes are in the same format except that the word length is 36 bits, while that of the B-5500 is 48 bits. The program accepts as input the two tapes containing the four digitized channels of FM/FM data and produces one tape containing all four channels. (At the present time, the digital input tapes are written in low density—200 bits per inch—on the tape, but this is not a limitation for the B-5500, which can read in either low or high density.) The flow diagram for this program is shown in Figure 10, while the reproduced Algol deck is shown in Appendix C.

Commutator Converter Program

This program differs slightly from the data conversion program in that it will only accept a single tape at a time as input. However, the basic logic is the same, and the output formats have similarities. The program converts the data tape generated by the ADC process, from a 36 bit word length to a 48 bit word length for use on the B-5500. The flow diagram is shown in Figure 11, while the reproduced Algol deck is presented in Appendix C. The program converts the word length and lists on the line printer periodically the tape block which is currently being written, and when the input data tape is exhausted, the output tape is rewound and periodically dumped to serve as a check on the conversion process by comparing this listing with the previous listing.

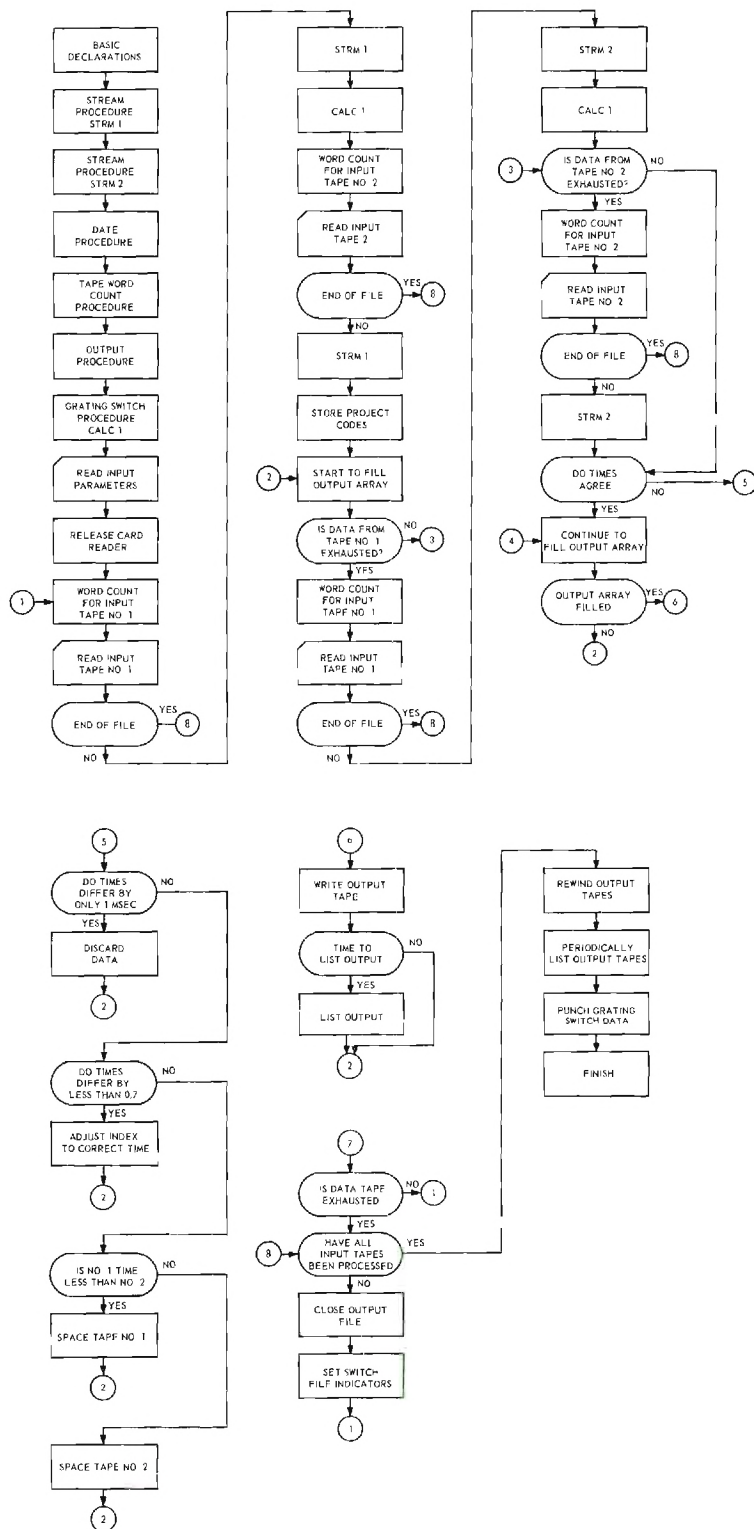


Figure 10. FM Data Converter Flow Chart.

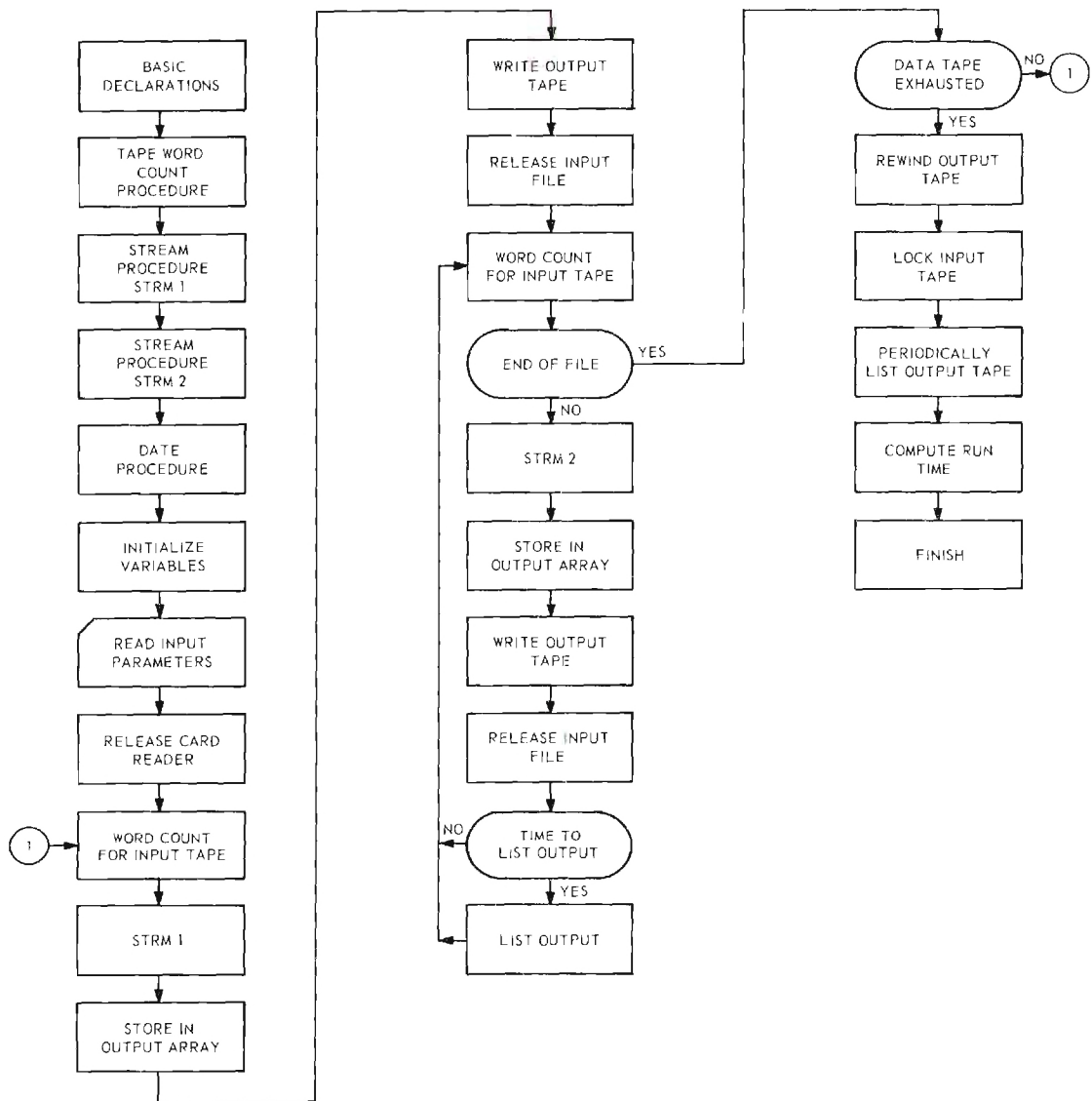


Figure 11. Commutator Converter Flow Chart.

Addition of Wave Length Program

The third program generates the input tape for the main data reduction program by providing the wave length at which a given data point was taken. During the FM data conversion process, the times at which the grating switch opened are punched onto cards. These times are then hand edited (to remove bad times and to include times which may have been missed by a malfunction of the grating switch) and used as input for the addition of wave length program. The output of the program is a tape with a similar format to the input tape (the output tape from the FM data conversion program), but with wave length added in bits 1 through 13. The flow diagram for this program is shown in Figure 12 while the reproduced Algol deck is in Appendix C.

Specific Problems in Data Reduction

After the completion of the addition of wave length to the FM data and conversion of the commutator data, two additional programs are needed to obtain the final answers. One, the commutator reduction program, reduces and lists the data that are contained on the commutator, such as scatter angle, battery voltages, error signals and temperatures. The other program obtains intensity and polarization parameters versus wave length. This second program also combines some of the results of the commutator reduction program so that the scatter angle and an "on-sun" flag are contained in the output. Each of these two programs will be discussed.

Commutator Reduction Program

The commutator reduction program uses the data from the commutator conversion program, averages it over a suitable time interval, converts the digital value to engineering units (degrees, volts, temperature, etc.),

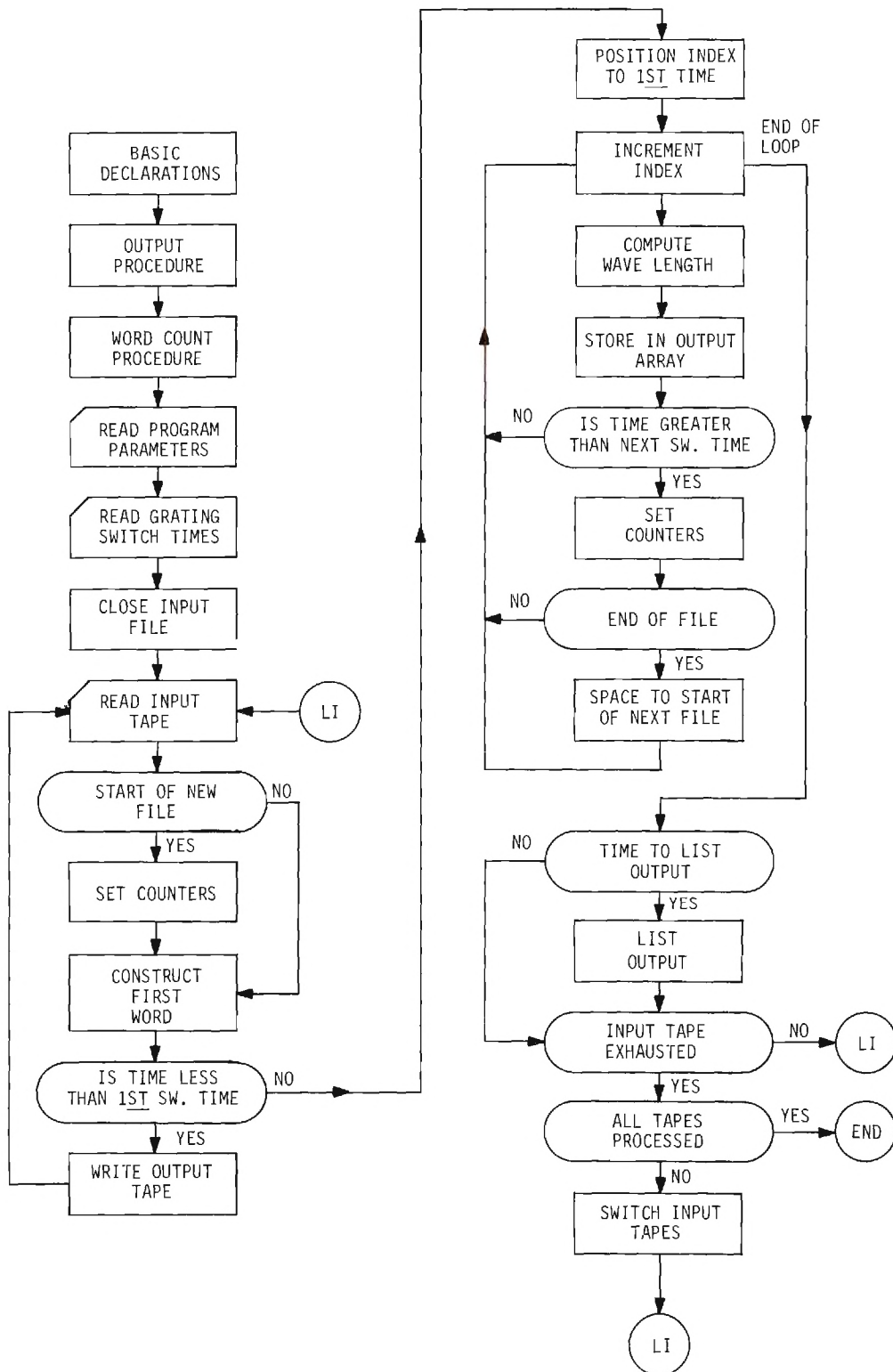


Figure 12. Addition of Wave Length Flow Chart.

and lists the output. For the 1 July 1965 flight, a list of commutator segments versus channel number (multiplex number, also) is given in Table 1. The maximum and the minimum signals (5.0 and 1.0 volts, respectively) are used for calibration purposes, and at present is the only calibration on the commutated data. The flow chart for this program is shown in Figure 13, while the Algol deck is reproduced in Appendix C.

Main Data Reduction Program

This final program in the chain produces the intensity and the modified Stokes parameters versus wave length for a specified time interval. A time correlation is used to obtain the altitude and scatter angle which have been derived elsewhere; the altitude is obtained from the launch organization, and the scatter angle is obtained from the commutator data. The program requires two input tapes: (1) the output tape from the addition of wave length program, and (2) an auxiliary input tape which contains certain constants which are used in the program, and also the temperature, altitude, and scatter angle profiles. Basically the program is similar to the calibration program, although it is not nearly as complex. The flow chart for this program is shown in Figure 14, while the reproduced Algol deck is contained in Appendix C.

This program has been used with a portion of the data obtained on the 1 July 1965 flight, and the results are shown graphically in Figures 15 and 16. Figure 15 shows the intensity of the scattered sunlight radiation at float altitude (121,000 feet) at approximately 71 degrees from the sun. Figure 16 shows the degree of polarization of the scattered sunlight under the same conditions. The calculation of the degree of polarization and the other modified Stokes parameters becomes inaccurate when the total

Table 1. Commutator Segments

Segment	
Number	Description
1	Maximum signal
2	Minimum signal
3	Solar monitor
4	Azimuth position
5	Elevation scan potentiometer
6	Pointing control Az CW error signal
7	Pointing control El CW error signal
8	Pointing control Az CCW error signal
9	Pointing control El CCW error signal
10	Electronics temperature
11	Optics temperature
12	Pointing control temperature
13	Ground plane temperature
14	Main battery temperature
15	TM battery temperature
16	Electronics battery temperature
17	TM battery voltage
18	Main battery voltage
19	Electronics battery voltage
20	Solar position photocall #1
21	Solar position photocall #2
22	Solar position photocall #3
23	Calibration light, electronics heater multiplex
24	Battery heater multiplex
25	Regulated 18 v. for pointing control
26	Camera pulse
27	Regulated 12 v. for thermistors
28	Reference voltage

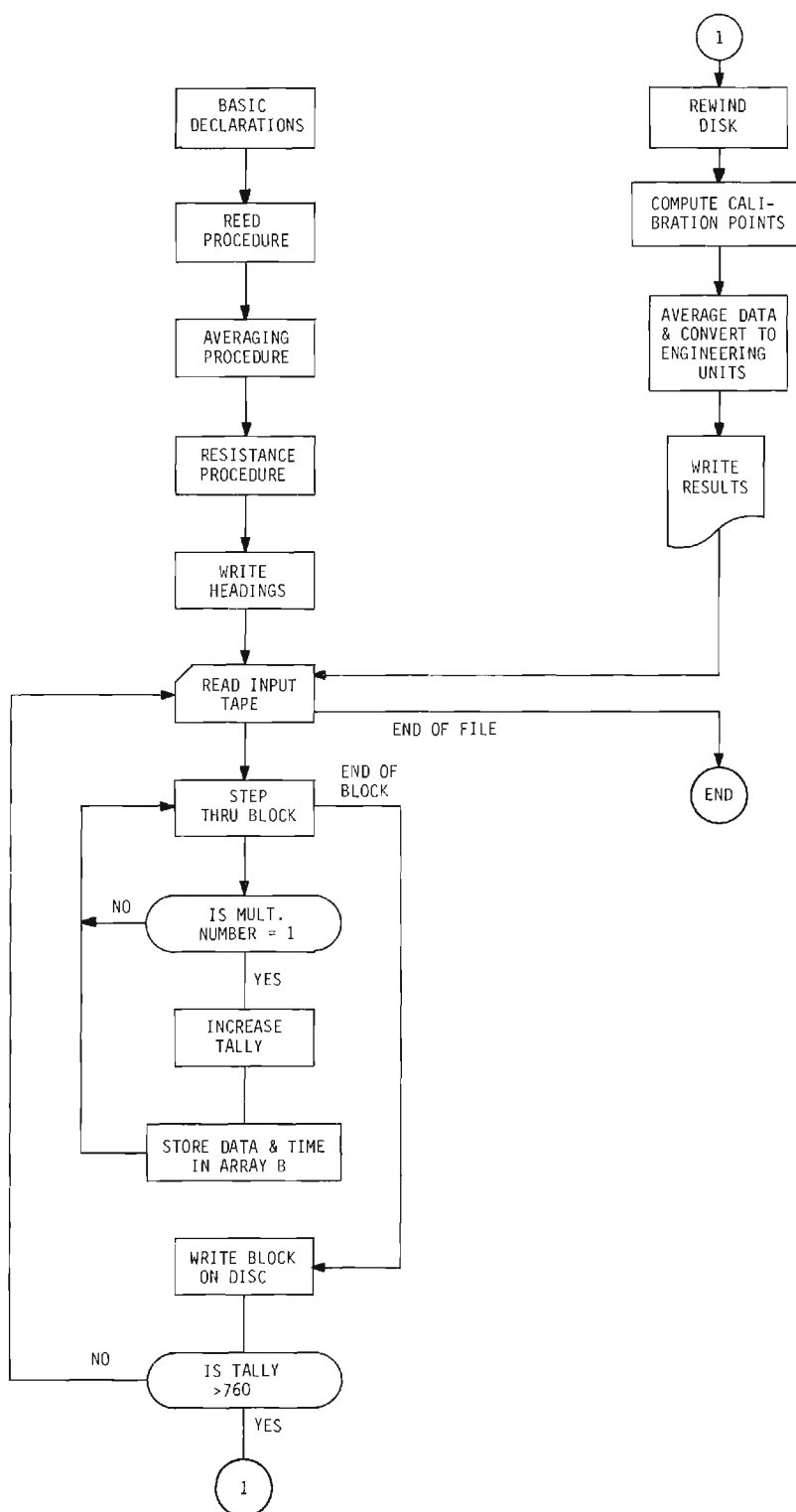


Figure 13. Commutator Reduction Flow Chart.

intensity is low, and hence, for those wave lengths where the intensity is low, the probable error on the other calculations increases. The ellipticity as determined by this method was never more than 0.03, and this figure could arise from computational errors and an inexact numerical approximation during the Fourier analysis of the photomultiplier tube signals. The angle of polarization was approximately horizontal. A detailed error evaluation has not been performed on the overall system, and therefore no estimate of probable error is available.

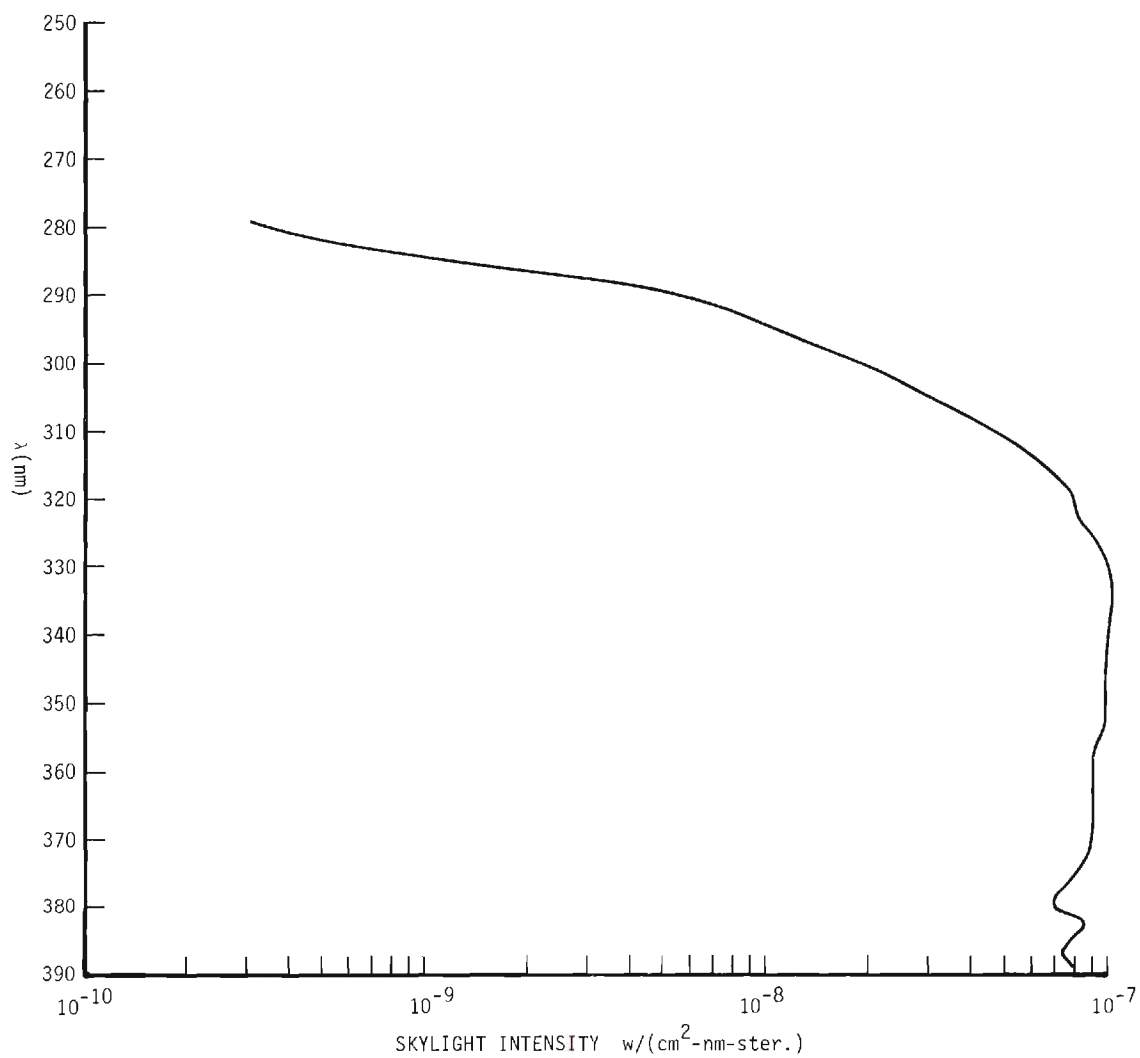


Figure 15. Spectral Intensity of a Portion of the UV Sky.

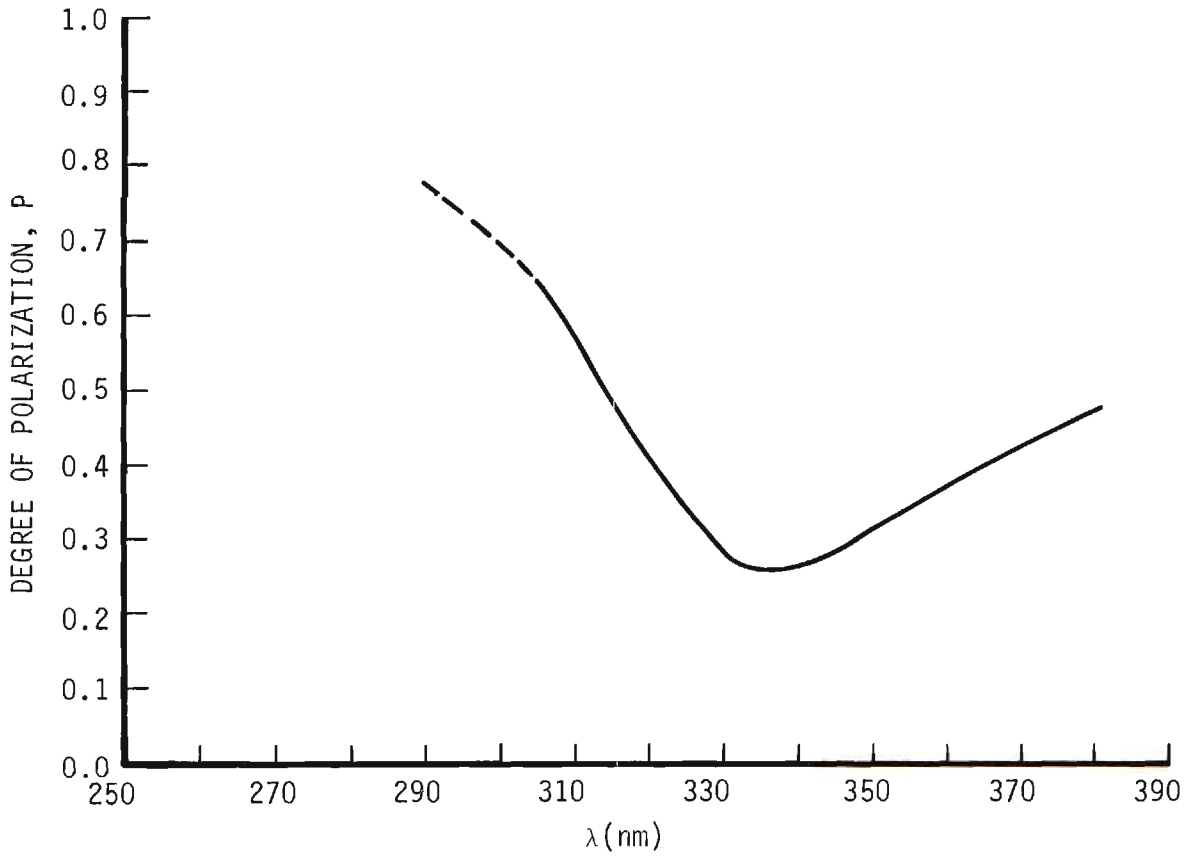


Figure 16. Degree of Polarization of a Portion of the UV Sky.

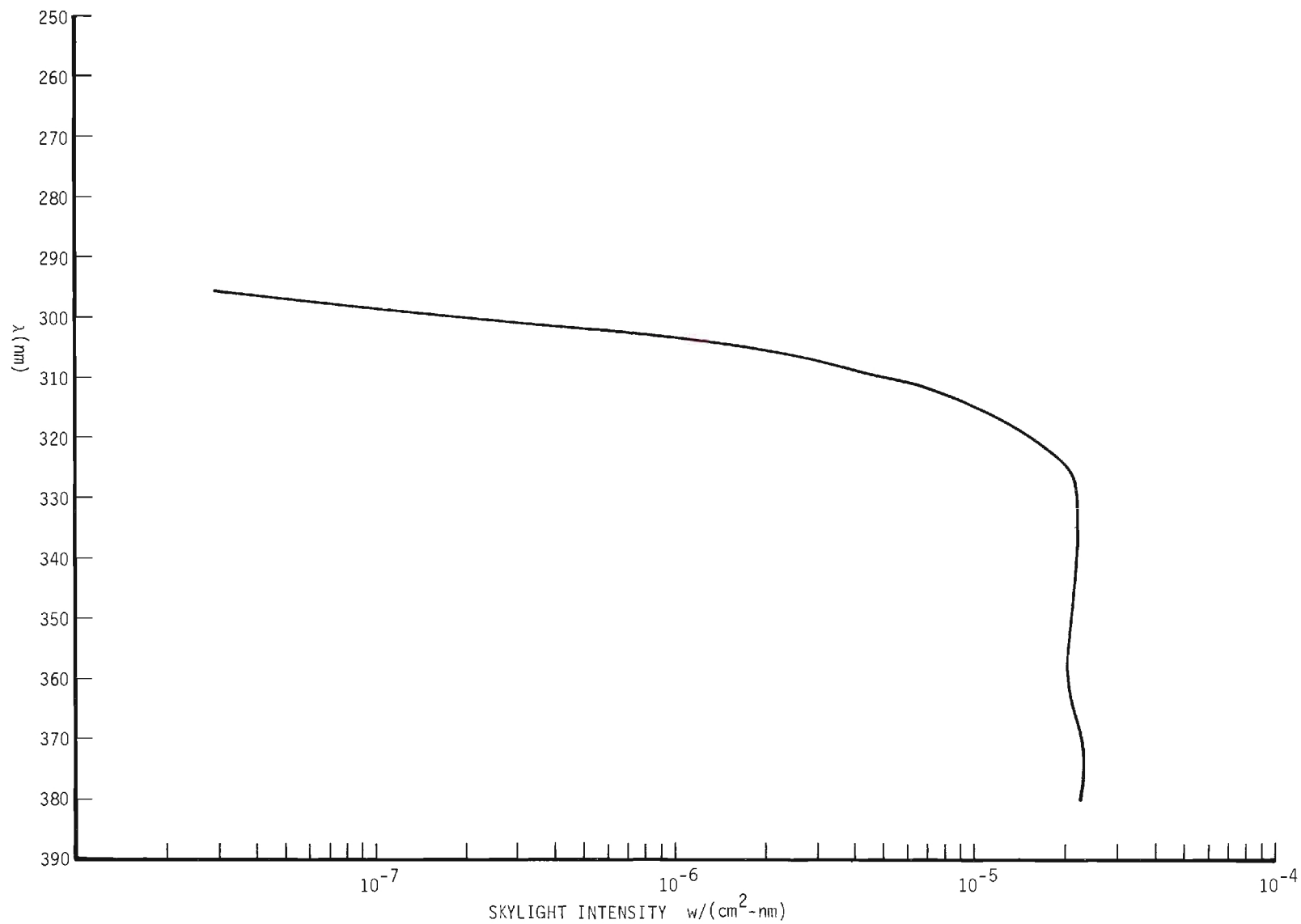


Figure 17. Spectral Intensity of the UV Sky Radiation.

CHAPTER V

SUMMARY AND CONCLUSIONS

The knowledge of the ultraviolet radiation incident from the sun and sky is of vital interest for geophysics as well as for biophysics. Considerable work has been done in the field from ground based observatories such as Davos, Switzerland, and the purpose of this experiment is to supplement these observations by taking data at high altitudes in a similar wave length region. The failure of the instrumentation package by the entanglement of the visibility flags on the 1 July 1965 flight prevented the acquisition of data from all scatter angles, but sufficient data were obtained to demonstrate the feasibility and practicality of the experiment. The results shown in Figures 15 and 16 agree with the experimental results of Bener⁸ (Figure 17) and also some of the theoretical results of Sekera³ regarding skylight intensity. It should be noted that Bener's data are taken for global sky radiation, whereas the data shown in Figures 15 and 16 are for an occluded angle of approximately 0.2 steradians. This agreement supports all phases of the experiment including calibration and data reduction, and it also shows that imperfect optical polarizing components can be successfully used in an Ebert-Fastie-Sekera arrangement to determine polarization and intensity.

Various improvements are possible to increase the accuracy, reliability, and performance of the overall system, although the basic design should remain intact. The data reduction programs can be improved and streamlined to reduce the amount of computer time necessary to reduce the

data completely. An additional program could be written to perform the editing of the grating switch times prior to the addition of wave length. A program could also be written to provide a time edit of the data to eliminate undesirable data points which have an error in time. A master data preparation program could be assembled from programs already in existence, or suggested, that uses as input the tapes as received from the analog-to-digital conversion and produces an output tape with time editing which is suitable as input to the final data reduction programs. Work is currently being performed along this line.

The results presented here were not the prime objective of this thesis, but rather were used to demonstrate that answers could be obtained through the data reduction chain that has been presented within the text of the thesis. A careful evaluation of these data and future data should be made to ascertain overall accuracy and probable error. Since the data presented represent only one small portion of the sky, no definite conclusions can be reached regarding the mapping of the sky intensity, but the conclusion can be made that the data reduction system produces the desired results.

APPENDIX A

STOKES VECTORS AND MUELLER CALCULUS

Completely or partially polarized light can be specified by a set of four quantities known as the Stokes parameters, all of which have the dimensions of intensity.⁹ These four parameters are usually represented by a column vector as:

$$\begin{bmatrix} I \\ Q \\ U \\ V \end{bmatrix} . \quad (\text{A-1})$$

The electromagnetic definitions of these quantities are

$$I = \langle e_x^2 + e_y^2 \rangle \quad (\text{A-2a})$$

$$Q = \langle e_x^2 - e_y^2 \rangle \quad (\text{A-2b})$$

$$U = \langle 2e_x e_y \cos \gamma \rangle \quad (\text{A-2c})$$

$$V = \langle 2e_x e_y \sin \gamma \rangle , \quad (\text{A-2d})$$

where e_x and e_y are the instantaneous x and y components of the electric field respectively, γ is the relative phase angle between e_x and e_y , and the brackets indicate a time average. The first parameter, I, is to be interpreted as the total intensity of the light, and the remaining Stokes parameters lead to the following inequality:

$$I^2 \geq Q^2 + U^2 + V^2 . \quad (\text{A-3})$$

The intensity is equal to the square root of the sum of the other three only if the beam is completely polarized, i.e., no unpolarized component present. It is convenient to define the degree of polarization, P , as:

$$P = \frac{(Q^2 + U^2 + V^2)^{\frac{1}{2}}}{I} \quad (\text{A-4})$$

If ϕ is the angle which the major axis of the elliptically polarized light (as a special case, linearly polarized light) makes with the reference axis, then

$$\begin{aligned} I &= I \\ Q &= PI \cos 2\phi \\ U &= PI \sin 2\phi \\ V &= V \end{aligned} \quad (\text{A-5})$$

and the quantities, I , P , V , and ϕ will be designated as the modified Stokes parameters. These do not all have the same dimensions, and therefore will not transform as the normal Stokes vector.

In Mueller calculus,¹⁰ an optical device is represented by a four by four matrix which operates on the Stokes vector of the incident light to give the Stokes vector of the transmitted (or reflected) light. For a non-perfect linear polarizer, let a and b be the fractional amplitude of transmission of the major and minor axis respectively (ideally, $a = 1$ and $b = 0$). The Mueller matrix for such a polarizer can be derived as follows: let m_{ij} be an element of the Mueller matrix M_P , and let it operate on completely unpolarized light.

$$\begin{bmatrix} m_{11} & m_{12} & m_{13} & m_{14} \\ m_{21} & m_{22} & m_{23} & m_{24} \\ m_{31} & m_{32} & m_{33} & m_{34} \\ m_{41} & m_{42} & m_{43} & m_{44} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} m_{11} \\ m_{21} \\ m_{31} \\ m_{41} \end{bmatrix} \quad (\text{A-6})$$

Now we expect the Stokes vector of the transmitted light to be (cf A-2)

$$\frac{1}{2} \begin{bmatrix} a^2 + b^2 \\ a^2 - b^2 \\ 0 \\ 0 \end{bmatrix}, \quad (\text{A-7})$$

and hence

$$m_{11} = \frac{1}{2}(a^2 + b^2) \quad (\text{A-8a})$$

$$m_{21} = \frac{1}{2}(a^2 - b^2) \quad (\text{A-8b})$$

$$m_{31} = m_{41} = 0 \quad (\text{A-8c})$$

(The factor of $\frac{1}{2}$ is for normalization). After making these substitutions into the Mueller matrix M_p , the matrix operates on light completely linearly polarized at 0° as follows:

$$\begin{bmatrix} \frac{1}{2}(a^2 + b^2) & m_{12} & m_{13} & m_{14} \\ \frac{1}{2}(a^2 - b^2) & m_{22} & m_{23} & m_{24} \\ 0 & m_{32} & m_{33} & m_{34} \\ 0 & m_{42} & m_{43} & m_{44} \end{bmatrix} \begin{bmatrix} 1 \\ 1 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} \frac{1}{2}(a^2 + b^2) + m_{12} \\ \frac{1}{2}(a^2 - b^2) + m_{22} \\ m_{32} \\ m_{42} \end{bmatrix} \quad (\text{A-9})$$

Here, we expect the Stokes vector to be

$$\begin{bmatrix} a^2 \\ a^2 \\ 0 \\ 0 \end{bmatrix}, \quad (\text{A-10})$$

so that

$$m_{12} = \frac{1}{2}(a^2 - b^2) \quad (\text{A-11a})$$

$$m_{22} = \frac{1}{2}(a^2 + b^2) \quad (\text{A-11b})$$

$$m_{32} = m_{42} = 0 \quad (\text{A-11c})$$

After these substitutions have been made into the Mueller matrix M_p , the matrix operates on completely linearly polarized light at 45° as follows:

$$\frac{1}{2} \begin{bmatrix} a^2 + b^2 & a^2 - b^2 & 2m_{13} & 2m_{14} \\ a^2 - b^2 & a^2 + b^2 & 2m_{23} & 2m_{24} \\ 0 & 0 & 2m_{33} & 2m_{34} \\ 0 & 0 & 2m_{43} & 2m_{44} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 1 \\ 0 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} a^2 + b^2 + 2m_{13} \\ a^2 - b^2 + 2m_{23} \\ 2m_{33} \\ 2m_{43} \end{bmatrix} \quad (\text{A-12})$$

Here we expect the transmitted vector to be

$$\begin{bmatrix} \frac{1}{2}(a^2 + b^2) \\ \frac{1}{2}(a^2 - b^2) \\ 2ab \\ 0 \end{bmatrix}. \quad (\text{A-13})$$

Hence

$$m_{13} = m_{23} = m_{43} = 0 \quad (\text{A-14a})$$

$$m_{33} = ab \quad (\text{A-14b})$$

As before, after making these substitutions and letting the resultant matrix operate on right circularly polarized light, we obtain:

$$\frac{1}{2} \begin{bmatrix} a^2 + b^2 & a^2 - b^2 & 0 & 2m_{14} \\ a^2 - b^2 & a^2 + b^2 & 0 & 2m_{24} \\ 0 & 0 & 2ab & 2m_{34} \\ 0 & 0 & 0 & 2m_{44} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} a^2 + b^2 + 2m_{14} \\ a^2 - b^2 + 2m_{24} \\ 2m_{34} \\ 2m_{44} \end{bmatrix} \quad (\text{A-15})$$

Here we expect the Stokes vector of the transmitted light to be

$$\begin{bmatrix} \frac{1}{2}(a^2 + b^2) \\ \frac{1}{2}(a^2 - b^2) \\ 0 \\ 2ab \end{bmatrix} \quad (\text{A-16})$$

and hence

$$m_{14} = m_{24} = m_{34} = 0 \quad (\text{A-16a})$$

$$m_{44} = ab \quad (\text{A-16b})$$

After making these substitutions, we divide the entire matrix M_P by a^2 , let $C_p = 1/2a^2$ and $r_p = b/a$ and obtain

$$M_P = C_p \begin{bmatrix} 1 + r_p^2 & 1 - r_p^2 & 0 & 0 \\ 1 - r_p^2 & 1 + r_p^2 & 0 & 0 \\ 0 & 0 & 2r_p & 0 \\ 0 & 0 & 0 & 2r_p \end{bmatrix}, \quad (\text{A-17})$$

where r_p is then the ratio of the amplitude of transmission of the minor to the major axes, and C_p is a normalization constant.

For an imperfect retardation plate of retardance δ which shows some linear polarization and is oriented with its fast axis along a reference axis (0°), we can derive the Mueller matrix as follows.

For the case of unpolarized incident light and light polarized at 0° , since there is no y component of the electric field to produce a relative phase shift, the development of the Mueller matrix M_R follows that for a linear polarizer thus:

$$M_R = \frac{1}{2} \begin{bmatrix} a^2 + b^2 & a^2 - b^2 & 2m_{13} & 2m_{14} \\ a^2 - b^2 & a^2 + b^2 & 2m_{23} & 2m_{24} \\ 0 & 0 & 2m_{33} & 2m_{34} \\ 0 & 0 & 2m_{43} & 2m_{44} \end{bmatrix} . \quad (A-18)$$

Letting this matrix operate on light polarized at 45° yields

$$\frac{1}{2} \begin{bmatrix} a^2 + b^2 & a^2 - b^2 & 2m_{13} & 2m_{14} \\ a^2 - b^2 & a^2 + b^2 & 2m_{23} & 2m_{24} \\ 0 & 0 & 2m_{33} & 2m_{34} \\ 0 & 0 & 2m_{43} & 2m_{44} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 1 \\ 0 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} a^2 + b^2 + 2m_{13} \\ a^2 - b^2 + 2m_{23} \\ 2m_{33} \\ 2m_{43} \end{bmatrix} . \quad (A-19)$$

From the electromagnetic definition of the Stokes vector, we would expect the transmitted light to appear as

$$\begin{bmatrix} \frac{1}{2}(a^2 + b^2) \\ \frac{1}{2}(a^2 - b^2) \\ 2ab \cos \delta \\ 2ab \sin \delta \end{bmatrix} , \quad (A-20)$$

and hence

$$m_{13} = m_{23} = 0 \quad (A-21a)$$

$$m_{33} = ab \cos \delta \quad (A-21b)$$

$$m_{43} = ab \sin \delta . \quad (A-21c)$$

After these substitutions are made in the Mueller matrix M_R , the matrix operates on right circularly polarized light to yield

$$\frac{1}{2} \begin{bmatrix} a^2 + b^2 & a^2 - b^2 & 0 & 2m_{14} \\ a^2 - b^2 & a^2 + b^2 & 0 & 2m_{24} \\ 0 & 0 & 2ab \cos \delta & 2m_{34} \\ 0 & 0 & 2ab \sin \delta & 2m_{44} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} a^2 + b^2 + 2m_{14} \\ a^2 - b^2 - 2m_{24} \\ 2m_{34} \\ 2m_{44} \end{bmatrix} \quad (A-22)$$

Again from the electromagnetic definition, we would expect the Stokes vector of the transmitted light to be

$$\begin{bmatrix} \frac{1}{2}(a^2 + b^2) \\ \frac{1}{2}(a^2 - b^2) \\ 2ab \cos (90 + \delta) \\ 2ab \sin (90 + \delta) \end{bmatrix} = \begin{bmatrix} \frac{1}{2}(a^2 + b^2) \\ \frac{1}{2}(a^2 - b^2) \\ -2ab \sin \delta \\ 2ab \cos \delta \end{bmatrix} . \quad (A-23)$$

Hence

$$m_{14} = m_{24} = 0 \quad (A-24a)$$

$$m_{34} = -ab \sin \delta \quad (A-24b)$$

$$m_{44} = ab \cos \delta . \quad (A-24c)$$

After making these final substitutions, we divide the entire matrix by a^2 , let $C_r = 1/2a^2$ and $r_r = b/a$ and obtain

$$M_R = C_r \begin{bmatrix} 1 + r_r^2 & 1 - r_r^2 & 0 & 0 \\ 1 - r_r^2 & 1 + r_r^2 & 0 & 0 \\ 0 & 0 & 2r_r \cos \delta & -2r_r \sin \delta \\ 0 & 0 & 2r_r \sin \delta & 2r_r \cos \delta \end{bmatrix} . \quad (A-25)$$

This is the Mueller matrix for an imperfect retardation plate with

its fast axis along the reference axis. It is then a simple matter to obtain the matrix for an arbitrary angle β by operating on (A-25) as follows:

$$M_{R\beta} = R [2\beta] [M_R] R [-2\beta] , \quad (\text{A-26})$$

where R is the well known rotation matrix

$$R[\alpha] = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \alpha & \sin \alpha & 0 \\ 0 & -\sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (\text{A-27})$$

Upon completion of this operation, the following is obtained:

$$\begin{aligned}
 [M_{R\beta}] = C_r & \begin{bmatrix}
 1 + r_r^2 & (1 - r_r^2) \cos 2\beta & (1 - r_r^2) \sin 2\beta & 0 \\
 (1 - r_r^2) \cos 2\beta & \frac{1}{2} \left(1 + r_r^2 + 2r_r \cos \delta \right) + & \frac{1}{2} \left(1 + r_r^2 - 2r_r \cos \delta \right) \sin 4\beta & 2r_r \sin \delta \sin 2\beta \\
 & \frac{1}{2} \left(1 + r_r^2 - 2r_r \cos \delta \right) \cos 4\beta & & \\
 (1 - r_r^2) \sin 2\beta & \frac{1}{2} \left(1 + r_r^2 - 2r_r \cos \delta \right) \sin 4\beta & \frac{1}{2} \left(1 + r_r^2 + 2r_r \cos \delta \right) - & -2r_r \sin \delta \cos 2\beta \\
 & & \frac{1}{2} \left(1 + r_r^2 - 2r_r \cos \delta \right) \cos 4\beta & \\
 0 & -2r_r \sin \delta \sin 2\beta & 2r_r \sin \delta \cos 2\beta & 2r_r \cos \delta
 \end{bmatrix} \quad (A-28)
 \end{aligned}$$

where β is the angle the fast axis makes with the reference axis, δ is the retardance of the phase plate, r_r is the ratio of the amplitudes of transmission of the fast to the slow axes, and C_r is a normalization constant.

APPENDIX B

DERIVATION OF THE CALIBRATION FORMULAE

After the operation indicated in equation (2) is performed, the intensity, I_A , of the light leaving the linear polarizer is detected by a photomultiplier tube, and this intensity is simply the first component of $[A]$. The signal out of the photomultiplier tube can be separated into components of β , the angle of rotation of the phase plate, as follows:

$$I_A = a_1 + a_2 \sin 2\beta + a_3 \cos 2\beta + a_4 \sin 4\beta + a_5 \cos 4\beta, \quad (B-1)$$

where

$$a_1 = CI \left[(1 + r_p^2)(1 + r_r^2) + \frac{1}{2}(1 - r_p^2)(1 + r_r^2 + 2r_r \cos \delta) P \cos 2\phi \right] \quad (B-2a)$$

$$a_2 = CI \left[(1 + r_p^2)(1 - r_r^2) P \sin 2\phi + 2Vr_r (1 - r_p^2) \sin \delta / I \right] \quad (B-2b)$$

$$a_3 = CI \left[(1 - r_p^2)(1 - r_r^2) + (1 + r_p^2)(1 - r_r^2) P \cos 2\phi \right] \quad (B-2c)$$

$$a_4 = \frac{1}{2}CI \left[(1 - r_p^2)(1 + r_r^2 - 2r_r \cos \delta) P \sin 2\phi \right] \quad (B-2d)$$

$$a_5 = \frac{1}{2}CI \left[(1 - r_p^2)(1 + r_r^2 - 2r_r \cos \delta) P \cos 2\phi \right] \quad (B-2e)$$

If the angle β is not known, but a relative angle, θ , is known, then

$$\beta = \theta + \zeta \quad (B-3)$$

and I_A can be expanded in terms of θ in the form

$$I_A = b_1 + b_2 \sin 2\theta + b_3 \cos 2\theta + b_4 \sin 4\theta + b_5 \cos 4\theta, \quad (B-4)$$

where

$$b_1 = a_1 \quad (B-5a)$$

$$b_2 = a_2 \cos 2\zeta - a_3 \sin 2\zeta \quad (B-5b)$$

$$b_3 = a_2 \sin 2\zeta + a_3 \cos 2\zeta \quad (B-5c)$$

$$b_4 = a_4 \cos 4\zeta - a_5 \sin 4\zeta \quad (B-5d)$$

$$b_5 = a_4 \sin 4\zeta + a_5 \cos 4\zeta. \quad (B-5e)$$

A Fourier analysis in terms of ϕ is now attempted on the b 's. As before, if the angle ϕ is not known, but a relative angle, ψ , is known, then

$$\phi = \psi + \eta, \quad (B-6)$$

and equation (B-5) can be placed in the following form:

$$b_1 = c_{11} + c_{12} \sin 2\psi + c_{13} \cos 2\psi \quad (B-7a)$$

$$b_2 = c_{21} + c_{22} \sin 2\psi + c_{23} \cos 2\psi \quad (B-7b)$$

$$b_3 = c_{31} + c_{32} \sin 2\psi + c_{33} \cos 2\psi \quad (B-7c)$$

$$b_4 = c_{42} \sin 2\psi + c_{43} \cos 2\psi \quad (B-7d)$$

$$b_5 = c_{52} \sin 2\psi + c_{53} \cos 2\psi, \quad (B-7e)$$

where

$$c_{11} = d_1 \quad (B-8a)$$

$$c_{12} = -d_2 \sin 2\eta \quad (B-8b)$$

$$c_{13} = d_2 \cos 2\eta \quad (B-8c)$$

$$c_{21} = d_3 \cos 2\zeta - d_5 \sin 2\zeta \quad (B-8d)$$

$$c_{22} = d_4 \cos 2\xi_1 = d_4 \cos 2(\eta - \zeta) \quad (\text{B-8e})$$

$$c_{23} = d_4 \sin \xi_1 = d_4 \sin 2(\eta - \zeta) \quad (\text{B-8f})$$

$$c_{31} = d_3 \sin 2\zeta + d_5 \cos 2\zeta \quad (\text{B-8g})$$

$$c_{32} = d_4 \sin 2\xi_1 = d_4 \sin 2(\eta - \zeta) \quad (\text{B-8h})$$

$$c_{33} = -d_4 \cos 2\xi_1 = -d_4 \sin 2(\eta - \zeta) \quad (\text{B-8i})$$

$$c_{42} = d_6 \cos 2\xi_2 = d_6 \cos 2(\eta - 2\zeta) \quad (\text{B-8j})$$

$$c_{43} = d_6 \sin 2\xi_2 = d_6 \sin 2(\eta - 2\zeta) \quad (\text{B-8k})$$

$$c_{52} = d_6 \sin 2\xi_2 = d_6 \sin 2(\eta - 2\zeta) \quad (\text{B-8m})$$

$$c_{53} = -d_6 \cos 2\xi_2 = d_6 \cos 2(\eta - 2\zeta) \quad , \quad (\text{B-8n})$$

where

$$d_1 = CI(1 + r_p^2)(1 + r_r^2) \quad (\text{B-9a})$$

$$d_2 = \frac{1}{2}CI(1 - r_p^2)(1 + r_r^2 + 2r_r \cos \delta) P \quad (\text{B-9b})$$

$$d_3 = 2VCIr_r (1 - r_p^2) \sin \delta \quad (\text{B-9c})$$

$$d_4 = CI(1 + r_p^2)(1 - r_r^2) P \quad (\text{B-9d})$$

$$d_5 = CI(1 - r_r^2)(1 - r_p^2) \quad (\text{B-9e})$$

$$d_6 = \frac{1}{2}CI(1 - r_p^2)(1 + r_r^2 - 2r_r \cos \delta) P \quad . \quad (\text{B-9f})$$

At a given wave length, I_A is determined for at least 25 different β . The plane of incident polarization, ψ , is then rotated by a fixed amount (in this case, 11.25°), and I_A is again measured for at least 25 different β , and this process is repeated until the plane of incident polarization has passed through at least 180° . Then, for each different angle of incident polarization, the b 's [equation (B-4)] are determined by a curve fitting process which produces a series of b_1 's, say, as a function of ψ as expressed in equation (B-7a). Another multiple linear regression is then performed on say, b_1 to determine c_{11} , c_{12} , c_{13} , and

after all the b's have been expanded in components of ψ , then all the c's would have been determined. It then follows from equation (B-8) that:

$$\eta = \frac{1}{2} \tan^{-1} \left(\frac{-c_{12}}{c_{13}} \right) \quad (\text{B-10})$$

$$\xi_1 = \frac{1}{2} \tan^{-1} \left(\frac{c_{23}}{c_{22}} \right) = \frac{1}{2} \tan^{-1} \left(\frac{c_{32}}{-c_{33}} \right) \quad (\text{B-11})$$

$$\xi_2 = \frac{1}{2} \tan^{-1} \left(\frac{c_{43}}{c_{42}} \right) = \frac{1}{2} \tan^{-1} \left(\frac{c_{52}}{-c_{53}} \right) \quad (\text{B-12})$$

$$\zeta = \eta - \xi_1 = \frac{1}{2}(\eta - \xi_2) \quad (\text{B-13})$$

Although it is possible to obtain the calibration parameters from the explicit form for the c's, it is somewhat more straight forward if the defining relationships of (B-3) and (B-6) are used, and the process is repeated by expanding I_A first in components of β as in (B-1) and then the a coefficients in terms of ϕ as

$$a_1 = d_1 + d_2 \cos 2\phi \quad (\text{B-14a})$$

$$a_2 = d_3 + d_4 \sin 2\phi \quad (\text{B-14b})$$

$$a_3 = d_5 + d_4 \cos 2\phi \quad (\text{B-14c})$$

$$a_4 = d_6 \sin 2\phi \quad (\text{B-14d})$$

$$a_5 = d_6 \cos 2\phi \quad . \quad (\text{B-14e})$$

From these relationships, the calibration parameters can be determined as follows:

$$r_r = \sqrt{\frac{1-k}{1+k}} \quad (\text{B-15})$$

$$\cos \delta = \frac{d_2 - d_6}{d_2 + d_6} \left(\frac{1 + r_r^2}{2r_r} \right) \quad (\text{B-16})$$

$$r_p = \sqrt{\frac{kd_1 - d_5}{kd_1 + d_5}} \quad (\text{B-17})$$

$$\text{CI} = \frac{d_1(1 + k)}{2(1 + r_p^2)} \quad , \quad (\text{B-18})$$

where

$$k = \frac{1 - r_r^2}{1 + r_r^2} = \sqrt{\frac{d_4 d_5}{d_1(d_2 + d_6)}} \quad (\text{B-19})$$

This effectively completes the optical calibration of the spectrophotopolarimeter.

APPENDIX C

COMPUTER PROGRAMS

This section contains the various computer programs that have been used in order to obtain data from the flight. It is assumed that the analog-to-digital conversion has been performed, and that the information is on magnetic tape. At present, six programs are necessary to completely reduce the data, and they are the FM Data Conversion, Commutator Conversion, Addition of Wave Length, Calibration Procedure, Commutator Reduction, and Main FM Reduction. Each of these will be discussed in detail.

FM Data Conversion Program

This program produces a tape which is compatible with the Burroughs B-5500 computer containing the FM data from all four channels--AC generator, grating switch, and the two photomultiplier tubes. The program also determines the times at which the grating switch opened, and these times are punched and listed as additional output. The program also lists the output tape periodically.

The program has as its input:

- (1) FILE FILL, in free field format, whether this is a test or run, the interval between records which are listed, the number of records at each interval to be listed, the number of pairs of input tapes (maximum 3), and the number of blocks or records to be converted (ignored if it is a production run),
- (2) FILE FFMD1, tape unit unlabeled tape, the digital tape containing the AC generator and grating switch data,

- (3) FILE FFMD2, tape unit, unlabeled tape, the digital tape containing the two photomultiplier tube signals.
- (4) FILE FFMD3, same as (2)
- (5) FILE FFMD4, same as (3)
- (6) FILE FFMD5, same as (2)
- (7) FILE FFMD6, same as (3)

Numbers (4) through (7) are only present if the number of pairs of input tapes is greater than one.

The program has as its output:

- (1) FILE FIL2, line printer, a listing of the data as it is converted, and then after the tape is rewound, a listing at the proper interval of the output tape,
- (2) FILE ZZZZZ01, labeled tape, a digital tape containing data, time, and multiplex number in a packed-word concept from the 1st pair of input tapes,
- (3) FILE ZZZZZ02, same as (2) except from the 2nd pair of input tapes,
- (4) FILE ZZZZZ03, same as (2) except from the 3rd pair of input tapes.

One block on the output tape contains one-half second of data. This arrangement permits easy positioning of the tape at a desired time. The data is stored on the output tape and the input tape in what is known as a packed-word, i.e., one computer word contains more than one word of information. The tapes as they are received are written in the following format:

Bits	0-10	Datum
	11-18	Time in seconds (maximum of 255)
	19-28	Time in milliseconds
	29-35	Multiplex number.

The datum which appears in the packed-word is the digital value in arbitrary units of the given multiplexer at the given time. The multiplex number is a number assigned by the ADC process to designate from which subcarrier the data were obtained. (On the commutated data tape, this number designates the segment from which the data are obtained.)

The output tape(s) are written in the following format:

Bits	0	Unused
	1-13	Wave length (to be added later)
	14-24	Data
	25-32	Time in seconds
	33-42	Time in milliseconds
	43-47	Multiplex number.

The record on the output tape is in the following form:

1st word	Bits	6-17	Number of words in the block
	Bits	18-23	File number
	Bits	24-35	The number of the wave length scan
	Bits	36-47	Block number
2nd word	Bits	30-46	High order time from 1st tape (seconds of day)
3rd word	Bits	30-46	High order time from 2nd tape (should agree with 2nd word)
4th word on			Data in the packed-word concept

On the first record on the tape, two additional words are placed after the ones described above. These are the project codes derived from the ADC process input tapes. These are placed at the end of the record so that the first portion of all the records will be identical. Since a large number of output tapes will be generated, it is anticipated that a label equation card would be used to equate the output files (ZZZZZ01, ZZZZZ02, and ZZZZZ03) to some other identifier. A label equation card equates the file identifier which is used in the program to a file identifier which will be read off an input file or written on an output file.

Commutator Converter Program

This program converts the digital tape which is obtained from the commutated data into a form suitable for the Burroughs computer. It has a similar logic pattern as the FM Data Conversion Program and the output is essentially identical. The program generates the output tape and periodically lists the tape so that the conversion process can be checked.

The program has as its input:

- (1) FILE FIL1, in free field format, the total number of blocks to be processed, the interval between the records which are to be listed, and the number of files on the input tape,
- (2) FILE FCMU, tape unit, unlabeled tape, the digital tape containing the commutated data.

If the entire tape is to be processed, the number of blocks to be processed is a number in excess of the number of blocks on the tape. There are usually around 5000 blocks on a tape, so as input, the number of blocks to be processed is conveniently placed at 99999999.

The program has as its output:

- (1) FILE FIL2, line printer, a listing of the data as they are converted at the interval specified by the input data on FIL1, and after the tape has been rewound, a listing, again at the proper interval, of the output tape (During the conversion process, when an end-of-file condition occurs on the input tape, the program writes the last block read of one file and the first block of the next file, but does not change the file identifier of the output file.),
- (2) FILE FDTCL, labeled tape, a digital tape written in the packed-word concept, containing a single file with all the input data included.

The data are recorded onto FDTCl in a packed-word which is of the following format:

Bits	0-13	Unused
	14-24	Data
	25-32	Time in seconds
	33-42	Time in milliseconds
	43-48	Multiplex number (commutator segment)

The first word in every record is the block number, and the second word contains the time of day in seconds in bits 30 through 46. The words from the third on to the end of the record contain the data in the packed-word as mentioned before. On the first record, however, the last word in the record is the project code.

Through a stream procedure, the number of words per record is automatically calculated by the computer. As a tape record is read into the buffer, a word count is generated in the first word prior to the start of the buffer. Thus, by referencing the buffer's starting address and going back one word, the number of words read can be made available to the computer. However, during the reading of the 36 bit word length tape, this is the number of 48 bit B-5500 words that are read and not the number of 36 bit words that are on the tape, thus, the number has to be converted before it is used.

The listing gives the time of day in hours, minutes, and seconds; time of day in seconds; number of words in the block to be listed; and the block number of output tape. If there are insufficient data to finish filling a row, zeroes are placed in the row to complete it.

A label equation card should be used if more than one tape is to be generated. Its use has already been described in the section of the FM Data Converter Program. In this case, the label equation card would

equate the file identifier which appears in the program, FDTCL, to a file identifier which would be written on the output tape.

With the use of the label equation card, it is believed that changes to the program itself would not be necessary. Therefore, the program was processed by the RECC library SQUEEZE routine for easier handling of the card deck. This program removes all comments and all non-essential spaces from the program, and thereby reduces the number of cards on which the program is written.

Addition of Wave Length Program

This program is the final link between the data tapes as they are received from the analog-to-digital conversion and the main data reduction program. This program calculates wave length and adds it to the data from the FM Data Conversion Program. The resulting tape is then used as input to the Main FM Reduction Program. This program also periodically lists the output to provide a check on the calculations.

The input file for the program is FIL3, and the data should be arranged in the following order:

Card Number	Columns	
1	1-4	Number of input tapes
	10-14	Interval between listings of output
2	1-7	Wave length at first opening
	10-17	Wave length at second opening
	20-27	Wave length at third opening
	30-37	Wave length at fourth opening
	40-47	Wave length at fifth opening
		(if present)
3	1-4	File number for present tape and scan
	10-14	Scan number
4,5,6,7,8	14-23	Times for switch openings.

Cards 3 through 8 are then repeated for all the switch opening times that are present.

The scan number is simply a tally of the number of complete wave length scans for a given file, and is used to distinguish one scan from another without having to resort to time as the indicator. The scan number and file number are used by the program for "bookkeeping" so that it can maintain the correct correlation between the input cards and the input tape. The output tape is in the same format as the input tape except for the construction of the first word in each record. This word is changed to the following format:

Bits	6-17	Number of words in the record
	18-23	File number corresponding to input file
	24-35	Scan number for the particular file being processed
	36-47	Block number.

The output of this program is periodically listed on the printer file, FIL2, as determined by the second entry on card 1. This listing is in a similar format to that used in the previous listings that have been produced. This format facilitates cross checking between input and output and also the checking of the overall performance of the addition of wave length program.

It is recognized that the hand editing that is required prior to the running of this program is a weak link in the data reduction chain. Present plans attempt to overcome this weakness and to make the data reduction completely handled by computers, but this program does provide the necessary results. Plans call for a program that does the editing task and computes the wave length which is then added to the output tape from the FM data conversion program.

Calibration Program

This program performs the operations derived in detail in Appendix B. The program essentially performs four Fourier analyses: 1) expanding the photomultiplier tube signals in terms of the angles which are determined from the AC generator, 2) expanding the components determined in the first step in terms of the relative angle of incident polarization, 3) re-expanding the photomultiplier tube signal in terms of the true angle of the retardation plates, and 4) re-expanding the components in terms of the true angle of incident polarization. The first two expansions are necessary to determine the relative phase angles involved in the AC generator and the incident polarization. The program uses an input tape containing the raw calibration data as they are generated by the Addition of Wave Length Program.

Input parameters to the program are in the following format, right justified:

	Columns	Description
Card 1	1-4	Number of angles of incident polarization
	5-8	Number of sample points per angle of incident polarization
	9-12	The number of wave lengths at which calibration is desired
Card 2	1-6	Starting time for calibration procedure
	7-12	Digitized value to indicate a change of angle of incident polarization
	13-18	Wave length below which only the 541F tube is calibrated
	19-24	Wave length above which only the 541A tube is calibrated
Card 3	1-10	Interval to dump program
	11-20	Approximate frequency of AC generator
	21-30	Incremental change of angle of incident polarization
	31-40	η for the 541F tube (if known)
	41-50	η for the 541A tube (if known)
	51-60	ζ for the 541F tube (if known)
	61-70	ζ for the 541A tube (if known)

	Columns	Description
Card 4	1-2	Compute option for first AC generator approximation
	3-4	Compute option for second AC generator approximation
	5-6	Compute option for first pass of PM current data
	7-8	Compute option for first pass of component data
	9-10	Compute option for second pass of PM current data
	11-12	Compute option for second pass of component data
	21-25	TRUE if the input data is to be listed, FALSE otherwise
	26-30	TRUE if times at which the calibration wave lengths occurred are to be listed, FALSE otherwise
	31-35	TRUE if AC generator frequency iterations are to be listed, FALSE otherwise
	36-40	TRUE if the AC generator frequency with correction calculations is to be listed, FALSE otherwise
	41-45	TRUE if the true AC generator frequency is to be listed, FALSE otherwise
	46-50	TRUE if calibration parameters are to be punched also, FALSE otherwise
	51-55	TRUE if card images are to be listed as punched, FALSE otherwise (only valid when preceding entry is TRUE)
	56-60	TRUE if ζ and η are known for 541F tube, FALSE otherwise
	61-65	TRUE if ζ and η are known for 541A tube, FALSE otherwise
Card 5	6 columns	Wave lengths at which calibration is desired. The number of wave lengths should match the third entry on card 1.

The constants η and ζ are defined by equations (B-6) and (B-3) respectively.

The compute option pertains to the least squares curvefitting procedure that it utilized in the program. If the option variable is 1, then only the curvefitting portion of the procedure is used. However, if the option variable is different from 1, the following actions take place:

Option variable	Action
2	Standard deviation is calculated and printed.
3	Standard deviation is calculated and printed, data lying outside a specified number of standard deviations is discarded, the curve-fitting procedure is again entered and standard deviation is calculated using this new data.
4	Same as 2 except that the input data is listed.
5	Same as 3 except that both sets of input data to the curvefitting procedure are listed.

If enough previous runs of the program have given a good indication of the value of ζ and η for either or both PM tubes, these data can be introduced for subsequent runs to eliminate the calculation of these quantities. The elimination of these computations can decrease the computer time necessary for a complete run. Data processor and input-output times are calculated and printed as the last item in the output. Past experience indicates that approximately 300 seconds are required for each tube at a given wave length if ζ and η are not known.

Commutator Reduction Program

This program examines the commutated data, averages it over a suitable time interval, converts the raw digital value to engineering units such as degrees, volts, etc., and prints the output. Basically the program executes a disk sort to extract the various multiplexers and arrange their values in an array. A suitable calibration of the various channels must be made prior to the running of the program so that this information may be included in the program.

The basic problem in this program is that the data are arranged on the input tape in serial form, i.e., ascending multiplex number, but in order for it to be manipulated, it must be in a parallel form, i.e., all

data of one multiplex number grouped together. The program utilizes a modified disk sort on the computer to accomplish this serial to parallel conversion. The program contains all calibrations of each segment including the nonlinear characteristic of the thermistors.

Some time prior to each flight a calibration was made on pertinent commutator channels. For those channels which measure a voltage, a known voltage was used as input, and the voltage out of the commutator segment was measured. A graph of these data was drawn relating voltage in versus voltage out. For the thermistor channels, the thermistors are subjected to different temperatures and their corresponding resistance is determined. Hence a relation between temperature and resistance is obtained. These data are contained in the program under a real procedure called RES(X). By determining the resistance, X, which is necessary to produce the voltage out of the commutator segment, and using this resistance as the input to the procedure, the procedure performs a tabular look up and produces a temperature which corresponds to the given resistance. For those commutator segments which measure an angle, a relation is derived between the angle and the voltage from the commutator segment, and this relation is used to obtain the desired angle.

In the program, double subscripted array B contains the data points for each segment in this manner: the first subscript is the segment or multiplex number (subscript 0 is the time), and the second subscript is the tally of the data points. The program reads the input tape, searches for segment #1, and fills array B[1, *] with its data point and fills array B[0, *] with the time. The data are then written on the disk. The program continues reading the input tape until 760 data points have been

read into the array. Subsequently, the disk is rewound, read and searched for segment #2 and the array is filled until the data on the disk are exhausted. The disk is then rewound, read and searched for segment #3, the array is filled, and so on until all twenty-eight segments are read and placed into the array. When array B is completely filled, the majority of the work is finished. The program subsequently uses array B, converts to a voltage and averages the values over a suitable number as shown below:

Segments	Averaged over:
1,2,10,11,12,13	
14,15,16,25,27	All 760 (approximately) samples
17,18,19,28	Every 150 samples
3,4,6,7,8,9,23,24	Every 75 samples
5	Every 25 samples

The averaging procedure uses all the data presented to it, calculates an average and the standard deviation. It then discards all data lying outside one standard deviation and reaverages the remaining data. The average voltage thus obtained is then applied to the particular calibration and the results of angle, voltage, or temperature are obtained.

Main FM Reduction Program

This program reduces the input data and obtains the intensity and the other Stokes parameters by performing a Fourier analysis of the photomultiplier tube currents in terms of the frequency of the AC generator and using the calibration constants that are also read into the program. An average wave length is calculated as well as the altitude and scatter angle. The output is listed for a given altitude and scatter angle (determined by the time) by intensity and the other modified Stokes parameters versus wave length. If the AC generator malfunctions, the program does not

attempt the Fourier analysis but rather does a simple averaging and flags the data as being qualitative and not quantitative.

In brief, the program reads in and initializes all essential constants and calibration parameters. Secondly, the program positions the main input tape to the correct starting time and fills a scratch tape with the data to be used in subsequent calculations. The program then uses this scratch tape as input, fills the proper arrays with the photomultiplier currents, AC generator signals, and wave length. The AC generator signal is then used to calculate the angular position of the phase plates, and then a Fourier analysis is made on the photomultiplier tube signals. After the components are determined, they are used to calculate the Stokes vector of the incident light.

The program requires as card input on file FILL the following information in the correct format:

Card 1	Columns	1-5	Starting time
		11-15	Stopping time
		21-24	Wave length interval for the samples
Card 2	Columns	1-5	Minimum value for the "shutter"
		11-15	Maximum value for the "shutter"
		21-26	1st tube shutter attenuation
		31-36	2nd tube shutter attenuation
		41-46	Approximate generator frequency
Card 3	Columns	1-7	1st tube generator phase angle
		11-17	2nd tube generator phase angle
		21-24	Minimum wave length for 2nd tube
		26-29	Maximum wave length for 1st tube
		31-33	Compute option for generator data
		34-36	Compute option for PM data
		37-41	Print option for generator data
		42-46	Print option for PM data

The "shutter" is an auxiliary slit which automatically covers the entrance slit of the spectrometer when the instrument is pointing close to the sun. It effectively reduces the amount of light entering each photo-

multiplier by the amount of the third and fourth entries on card 2. The minimum wave length for the second tube (third entry, card 3) is that wave length below which only the short wave length tube is used to obtain data. Similarly, the maximum wave length for the first tube is that wave length above which only data from the longer wave length tube is used. The compute option is the same as listed in the calibration program, but the print option (Boolean) determines if debugging and checking data is to be printed as well as the final results. If it is felt that the program is performing properly, then both print options should be set to FALSE, and the output would then consist of simply a listing of wave length versus the modified Stokes parameters.


```

COMMENT -- COMMUTATOR CONVERTER PROGRAM
BEGIN INTEGER I,J,K,M,N,K1,K2,PROJCODE,BLOCK,P, IFIL, IFIL1,TS
      REAL RNTIM, RNTIM1
      LABEL L1, L2, L3, L4, L0
      SAVE ARRAY A[0:500] ; ALPHA ARRAY B[0:600]
      ARRAY UI[0:250]
STREAM PROCEDURE TST1(A,B); BEGIN SI←A;DI←B;SI←SI-8;DS←8 CHR END
STREAM PROCEDURE STRM1(A,B,I,J,K);VALUE I,J,K;BEGIN SI←A;DI←B;
+DI←2;DS←6 CHR;DI←DI+5;DS←3 CHR;SI←SI+3;I(J(DI←DI+2;DS←6 CHR));K(DI←DI+2
+DS←6 CHR) END;STREAM PROCEDURE STRM2(A,B,I,J,K);VALUE I,J,K;BEGIN SI←A;
DI←B;DI←DI+5;DS←3 CHR;SI←SI+3;I(J(DI←DI+2;DS←6 CHR));K(DI←DI+2;DS←6 CHR)
END;PROCEDURE OUT1(A,N,FILEID);VALUE N;INTEGER N;FILE FILEID;ALPHA ARRAY
A[0];BEGIN INTEGER I,J,TH,THR,TMIN,TSEC;ARRAY B[ 1:12];FORMAT OUT FMT1(
I2, " HOURS", I3, " MINUTES", I3, " SECONDS",X10,I10,X45,"BLOCK NUMBER ",
I8),FMT2(4(F3.0,X1,F8.3,X1,F7.1,X9
))FOR I←1 DO BEGIN TM←A[I]
. [30:17];THR←TM DIV 3600;TMIN←(TM-3600×THR) DIV 60;TSEC←TM-3600×THR-60×T
MIN;WRITE(FILEID,FMT1,THR,TMIN,TSEC,TM,A[0])END;FOR I←3 STEP 4 UNTIL N
DO BEGIN FOR J←0 STEP 1 UNTIL 3 DO BEGIN
IF (I+J)>N THEN A[I+J]←0;
B[3×J+1]←A[I+J].[43:5]×1.0;B[3
×J+2] ← A[I+J].[25:8]+A[I+J].[33:10]/1000;B[3×J+3]←A[I+J].[14:11]×1.0
END;WRITE(FILEID,FMT2,FOR J←1 STEP 1 UNTIL 12 D
O B[J]) END;END OUT1
      FORMAT OUT FMT0 ("RUN TIME ", F12.5, "SECONDS"),
      FMT1 (X90, "PROJECT CODE ",I11),
      FMT2(X56, "WORD COUNT ",I5)
      FILE IN FIL1 (1,10), FCMU (1, 200)
      FILE OUT FIL2 1 (1,15)
      FILE FDT01 2 (1,800)
PROCEDURE DATE(FILEID)
      FILE FILEID
BEGIN ALPHA D ; INTEGER I, DAY, YR
      INTEGER ARRAY MO[1:12]
      FORMAT OUT FMT("RUN DATE ", I2,"/",I2,"/",I2)
      FILL MO[*] WITH 31, 28,31,30,31,30,31,31,30,31,30,31
      D ← TIME(0)
      YR ← 10×D.[18:6] + D.[24:6]

```

```

DAY ← 100×D.[30:6] + 10×D.[36:6] + D.[42:6] ;
I ← 0 ;
FOR I ← I+1 WHILE (DAY > 0) DO BEGIN ;
    DAY ← DAY - MO[I] ;
    IF ((YR MOD 4) = 0) THEN IF (I=2) THEN DAY←DAY+1 END ;
DAY ← DAY + MO[I] ;
I ← I - 1 ;
WRITE(FILEID, FMT, I, DAY, YR) END DATE ;
RNTIM ← TIME(2) ;
DATE(FIL2) ;
IFIL ← 0 ;
BLOCK ← 0 ;
READ (FIL1, /, M, P, IFIL1) ;
CLOSE (FIL1, RELEASE) ;
L0: READ (FCMU[NO], 1, U[*])[L2:L0] ;
TST1 (FCMU(0), TS) ;
N ← 4×((TS ) DIV 3) + (TS ) MOD 3 ;
WRITE (FIL2[NO], FMT2, N) ;
K1 ← (N-2) DIV 63 ;
K2 ← (N-2) MOD 63 ;
STRM1 (FCMU(0), A[0], K1, 63, K2) ;
FOR I ← N-1 STEP -1 UNTIL 2 DO BEGIN ;
    B[I+1].[14:29] ← A[I].[12:29] ;
    B[I+1].[43:5] ← A[I].[43:5] ;
    B[I+1].[12:2] ← 0 END ;
B[2] ← B[1] ← A[1] ;
B[N+1] ← A[0] ;
B[0] ← BLOCK ← BLOCK + 1 ;
WRITE (FDTCT, N+2, B[*]) ;
OUT1(B, N , FIL2) ;
RELEASE (FCMU) ;
L1: READ (FCMU[NO], 1, U[*])[L2:L1] ;
TST1 (FCMU(0), TS) ;
N ← 4×(TS DIV 3) + TS MOD 3 ;
K1 ← (N-1) DIV 63 ;
K2 ← (N-1) MOD 63 ;
STRM2 (FCMU(0), A[0], K1, 63, K2) ;

```

FOR I ← N-1 STEP -1 UNTIL 1 DO	BEGIN
R[I+2].[14:29] ← A[I].[12:29]	;
B[I+2].[43:5] ← A[I].[43:5]	;
B[I+2].[12:2] ← 0	END
BLOCK ← BLOCK + 1	;
B[2] ← B[1] ← A[0]	;
B[0] ← BLOCK	;
WRITE (FDTCl, N+2, B[*])	;
RELEASE (FCMU)	;
IF (BLOCK MOD P) = 0	THEN
BEGIN	
WRITE (FIL2[NO], FMT2, N)	;
OUT1 (B, N+1, FIL2)	;
END ;	
IF (BLOCK ≤ M)	THEN
GO TO L1	;
L2: IFIL ← IFIL + 1	;
WRITE (FIL2[NO], FMT2, N)	;
OUT1 (B, N+1, FIL2)	;
IF IFIL < IFIL1 THEN GO TO L0	;
REWIND (FDTCl)	;
LOCK (FCMU, RELEASE)	;
RNTIM1 ← (TIME(2) - RNTIM)/60	;
WRITE (FIL2, FMT0, RNTIM1)	;
READ (FDTCl[NO], 1, U[*])	;
TST1 (FDTCl(0), N)	;
READ (FDTCl, N, B[*])	;
PROJCODE ← B[N-1]	;
WRITE (FIL2[PAGE]) ;	;
WRITE (FIL2, FMT1, PROJCODE)	;
SPACE (FDTCl, -1)	;
WRITE (FIL2[NO], FMT2, N)	;
N ← N - 1 ;	;
L3: OUT1 (B, N-1, FIL2)	;
SPACE (FDTCl, P-1)[L4]	;
TST1(FDTCl(0), N)	;
READ (FDTCl, N, B[*])[L4]	;

```

        WRITE (FIL2(NO1), FMT2, N)           ;
        GO TO L3                             ;
L4:     LOCK (FDT01, RELEASE)                 ;
        RNTIM + (TIME(2) - RNTIM)/60          ;
        WRITE (FIL2, FMT0, RNTIM)            ;
END .

```

```

COMMENT -- FM DATA CONVERTER PROGRAM ;
BEGIN INTEGER I,N,N1,N2,K1,K2,P,P1,TP,M,IFIL, IFL1,IF1,LBL,J1,J2,K3,K4, ;
IPAR ;
REAL RNTIM, RNTIM1, TM1, TM2, TM3, TM4 ;
ARRAY CT1, CT2[0:6], TIM[1:2,0:3,0:350], VAL[0:8] ;
INTEGER ARRAY IFL[0:6] ;
SAVE ARRAY A,B[0:275] ;
ALPHA ARRAY DT[0:1022] ;
BOOLEAN Z ;
LABEL LFIL,LEND,L1,L1A,L1B,L2,L2B,L3,L4,LP1,LP2,LP3,LP4,LP5,LP6, ;
LA, LP1A, LP3A, LP5A, LP7A, LP4A, LP6A, L1C, L1D, L5 ;
LABEL L8,L9,L10,L11 ;
SAVE FILE IN FFMD1 2 (1,250), FFMD2 2 (1,250), FFMD3 2 (1,250), ;
FFMD4 2 (1,250), FFMD5 2 (1,250), FFMD6 2 (1,250) ;
FILE OUT ZZZZZ01 2 (1,1023, SAVE 100), ;
ZZZZZ02 2 (1,1010, SAVE 30), ;
ZZZZZ03 2 (1,1010, SAVE 30) ;
FILE IN FIL7 (1,10) ;
FILE OUT FIL2 6 (2,15) ;
FILE OUT FILP1 2 (1,10, SAVE 1) ;
SWITCH FILE SWI1 := FFMD1, FFMD3, FFMD5 ;
SWITCH FILE SWI2 := FFMD2, FFMD4, FFMD6 ;
SWITCH FILE SWD1 := ZZZZZ01, ZZZZZ02, ZZZZZ03, ZZZZZ01, ZZZZZ01, ;
ZZZZZ01 ;
STREAM PROCEDURE STRM1(A,B,I,J,K) VALUE I,J,K BEGIN SI:=A;DI:=B ;
SI:=SI+2;DI:=DI+4;DS:=4 CHR;DI:=DI+5;DS:=3 CHR;SI:=SI+3 ;
I(J(DI:=DI+2;DS:=6 CHR));K(DI:=DI+2;DS:=6 CHR) END ;
STREAM PROCEDURE STRM2(A,B,I,J,K) VALUE I,J,K BEGIN SI:=A;DI:=B ;
DI:=DI+5;DS:=3 CHR;SI:=SI+3 ;
I(J(DI:=DI+2;DS:=6 CHR));K(DI:=DI+2;DS:=6 CHR) END ;
PROCEDURE DATE(FILE1) ;FILE FILE1 ;BEGIN ALPHA D;INTEGER I,DY,YR ;
INTEGER ARRAY MO[1:12];FORMAT OUT F1("RUN DATE " I2,"/" I2,"/" I2/) ;
FILL MO[*] WITH 31,28,31,30,31,30,31,31,30,31,30,31; D:=TIME(0) ;
YR:=10XD.[18:6]+D.[24:6];DY:=100XD.[30:6]+10XD.[36:6]+D.[42:6]-1 ;
I:=0;FOR I:=I+1 WHILE DY>0 DO BEGIN DY:=DY-MO[I];IF YR MOD 4=0 THEN ;
IF I=2 THEN DY:=DY-1 END;I:=I-1;DY:=DY+MO[I];WRITE(FILE1,F1,I,DY,YR)END; ;
INTEGER PROCEDURE WORD(F1, LBL) ; FILE F1 ; INTEGER LBL ;

```



```

BEGIN LABEL L1,L2,L3 ;
  INTEGER I ; ARRAY A[0:2] ; STREAM PROCEDURE S1(A,B) ; BEGIN
SI:=A;DI:=B;SI:=SI-8;DS:=8 CHR END; READ(F1[NO],I,A[*])[L1:L2] ;
  S1(F1(0),I) ; LBL := 0 ; WORD := I ; GO TO L3 ;
  L1: LBL := 1 ; GO TO L3 ; L2: LBL := 2 ; L3: END ;
PROCEDURE OUT2(A,N,F1) ; VALUE N ; INTEGER N ; FILE F1 ; ALPHA ARRAY A[0] ;
BEGIN INTEGER I,J,TM,T1,T2,T3 ; INTEGER ARRAY B[0:20] ; FORMAT OUT FMT1(I2,"
HOURS",I3," MINUTES",I3," SECONDS",X10,"TIME ",I6,X44,"BLOCK NUMBER ",I
3,"-",I4),FMT2(4(I2,X2,I3,".",I3,X2,I4,".0",X7)) ;
  J := A[0].[12:6] ;
FOR I:=1,2 DO BEGIN TM:=A[I].[30:17] ; T1:=TM DIV 3600 ; T2:=(TM-3600×T1) DIV
60 ; T3:=TM-3600×T1-60×T2 ; WRITE(F1,FMT1,T1,T2,T3,TM,J,A[0].[18:30]) END ;
FOR I:=3 STEP 4 UNTIL N=3 DO BEGIN FOR J:=0,1,2,3 DO BEGIN IF I+J>N THEN A
[I+J]:=0 ; B[4×J]:=A[I+J].[43:5] ;
  B[4×J+1]:=A[I+J].[25:8] ;
  B[4×J+2]:=A[I+J].[33:10] ;
  B[4×J+3]:=A[I+J].[14:11] ;
  WRITE(F1,FMT2,FOR J:=0 STEP 1 UNTIL 15 DO B[J]) END END ;
FORMAT OUT FMTA("ACCUMULATED RUN TIME ",F8.2),
  FMTB(X90,"PROJECT CODE ",I8),
  FMTC(X57,"WORD COUNT ",I5),
  FMTD("PARITY ERROR IN NEXT BLOCK AFTER ",I3,"-",I4,
  " ; TIMES: ",I5," ",I5),
  FP1("XXX PARITY ERROR, INPUT TAPE 1, FILE # ",I3),
  FP2("XXX PARITY ERROR, INPUT TAPE 2, FILE # ",I3),
  FP3("XXX PARITY ERROR, INPUT TAPE 1, STEP 2, FILE#",I3),
  ,FP4("XXX PARITY ERROR, INPUT TAPE 2, STEP 2, FILE#",I3),
  ,FP5("XXX PARITY ERROR, OUTPUT TAPE, STEP 1, FILE#",I3),
  ,FP6("XXX PARITY ERROR, OUTPUT TAPE, STEP 2, FILE#",I3) ;
PROCEDURE CALC1(N) ;
  VALUE N ;
  INTEGER N ;
BEGIN INTEGER I,I1,I2,J,K ;
  REAL TM,T ;
OWN BOOLEAN Z ;
  LABEL L1,L2 ;
  OWN ARRAY B[0:1,0:10] ;

```

```

FORMAT OUT FMTP ("01", X2, I2, X2, I3, X2, F9.3, " GRATING",X50),
              FMTR ("02", X2, I2, X2, I3, X2, F9.3, " CALIBRATION",
                  X46)
;
TM ← A[I2].[30:17] - A[2].[23:8]
;
FOR I := 4 STEP 4 UNTIL N-1 DO BEGIN
    T ← A[I].[12:11]
    ;
    J ← 8
    ;
    DO J ← J - 1 UNTIL T ≥ VAL[J]
    ;
    FOR I1 := 0,1 DO
        FOR K := 1 STEP 1 UNTIL 9 DO
            B[I1,K-1] := B[I1,K]
            ;
        B[0,9] ← J
        ;
        B[1,9] ← TM + A[I].[23:8] + A[I].[31:10]/1000
        ;
        FOR J := 1,3,5 DO BEGIN
            FOR I1 := 0 STEP 1 UNTIL 4 DO
                IF B[0,I1] ≠ J THEN
                    GO TO L1
            ;
            FOR I1 := 5 STEP 1 UNTIL 9 DO
                IF B[0,I1] ≠ J-1 THEN
                    GO TO L1
            ;
            CT1[IFIL] := CT1[IFIL] + 1
            ;
            TIM[1,IFIL,CT1[IFIL]] := B[1,5]
            ;
            WRITE (FILP1, FMTP, IFIL, CT1[IFIL], TIME[1,IFIL,CT1[IFIL]])
            ;
            Z := FALSE
            ;
L1:
            IF NOT Z THEN BEGIN
                FOR I1 := 0 STEP 1 UNTIL 3 DO
                    IF B[0,I1] ≥ 4 THEN
                        GO TO L2
                ;
                FOR I1 := 6 STEP 1 UNTIL 9 DO
                    IF (B[0,I1] < 4) OR (B[0,I1] > 5) THEN
                        GO TO L2
                ;
                Z := TRUE
                ;
                CT2[IFIL] := CT2[IFIL] + 1
                ;
                TIM[2,IFIL,CT2[IFIL]] := 3.0 + B[1,5]
                ;
                WRITE (FILP1, FMTR, IFIL, CT2[IFIL], TIME[2,IFIL,CT2[IFIL]])
                ;
L2:
            END
        END
    END

```

```

END
RNTIM := TIME(2)
DATE(FIL2)
IPAR := 0
READ (FIL7, /, FOR I:=0 STEP 1 UNTIL 7 DO VAL[I])
READ (FIL7, /, Z, P, P1, TP, M)
READ (FIL7, /, FOR I:=0 STEP 1 UNTIL TP-1 DO IFL[I])
IF1 := 0
READ (FIL7, /, I)[L1B]
IF1 := 3
L1B: CLOSE (FIL7, RELEASE)
LP1A: DT[0] := 0
LFIL: N1 := WORD (SWI1[IFIL], LBL)
IF LBL=1 THEN GO TO L8 ELSE IF LBL=2 THEN GO TO LP1
DT[0],[12:6] ← IFL1 + 1
N1 := 4×(N1 DIV 3) + N1 MOD 3
K1 := (N1-2) DIV 63
K2 := (N1-2) MOD 63
STRM1 (SWI1[IFIL](0), A[0], K1, 63, K2)
CALC1(N1)
RELEASE (SWI1[IFIL])
LA: N2 := WORD (SWI2[IFIL], LBL)
IF LBL=1 THEN GO TO L9 ELSE IF LBL=2 THEN GO TO LP2
N2 := 4×(N2 DIV 3) + N2 MOD 3
K1 := (N2-2) DIV 63
K2 := (N2-2) MOD 63
STRM1 (SWI2[IFIL](0), B[0], K1, 63, K2)
RELEASE (SWI2[IFIL])
K3 := A[1]
K4 := B[1]
DT[1003] := A[0]
DT[1004] := B[0]
J1 := J2 := 2
LP3A:
L1: N ← IF DT[0],[18:30] = 0 THEN 5 ELSE 3
FOR I := 0 STEP 2 UNTIL 498 DO

```

BEGIN


```

L1C:      IF I+J1+2 > N1                                THEN BEGIN
          J1 := 1-I
          N1 := WORD (SWI1[IFIL], LBL)
          IF LBL=1 THEN GO TO L10 ELSE IF LBL=2 THEN GO TO LP3
          N1 := 4*(N1 DIV 3) + N1 MOD 3
          K1 := (N1-1) DIV 63
          K2 := (N1-1) MOD 63
          STRM2 (SWI1[IFIL](0), A[0], K1, 63, K2)
          TM3 ← A[0].[30:17] - A[1].[23:8]
          CALC1(N1)
          RELEASE (SWI1[IFIL])
          END
L1A:      IF I+J2+2 > N2                                THEN BEGIN
          J2 := 1-I
          N2 := WORD (SWI2[IFIL], LBL)
          IF LBL=1 THEN GO TO L11 ELSE IF LBL=2 THEN GO TO LP4
          N2 := 4*(N2 DIV 3) + N2 MOD 3
          K1 := (N2-1) DIV 63
          K2 := (N2-1) MOD 63
          STRM2 (SWI2[IFIL](0), B[0], K1, 63, K2)
          TM4 ← B[0].[30:17] - B[1].[23:8]
          RELEASE (SWI2[IFIL])
          END
          IF A[I+J1] = 0                                THEN BEGIN
              TM1 ← TM1 + 256.0
              J1 := J1 + 1
              GO TO L1C
          END
          IF B[I+J2] = 0                                THEN BEGIN
              TM2 ← TM2 + 256.0
              J2 := J2 + 1
              GO TO L1A
          END
          IF I = 0                                        THEN
              IF DT[0].[18:30] = 0                      THEN BEGIN
                  K3 ← A[1].[30:17]-A[2].[23:8]
                  K4 ← B[1].[30:17]-B[2].[23:8]
                  END
                  ELSE BEGIN
                      K3 ← A[0].[30:17]-A[1].[23:8]
                      K4 ← B[0].[30:17]-B[1].[23:8]
                      END
                  DT[2×I+3].[14:29] := A[I+J1 ].[12:29]

```

```

DT[2×I+3],[43:5] := A[I+J1 ],[43:5] ;
DT[2×I+4],[14:29] := A[I+J1+1],[12:29] ;
DT[2×I+4],[43:5] := A[I+J1+1],[43:5] ;
DT[2×I+5],[14:29] := B[I+J2 ],[12:29] ;
DT[2×I+5],[43:5] := 3 ;
DT[2×I+6],[14:29] := B[I+J2+1],[12:29] ;
DT[2×I+6],[43:5] := 4 ;
TM1 ← DT[2×I+3],[25:8] + DT[2×I+3],[33:10]/1000 + TM3 ;
TM2 ← DT[2×I+5],[25:8] + DT[2×I+5],[33:10]/1000 + TM4 ;
IF TM1 ≠ TM2 THEN BEGIN
    IF ABS(TM1-TM2) = 0.001 THEN
        GO TO L5 ;
    IF ABS(TM1-TM2) ≤ 0.700 THEN BEGIN
        IF TM1 > TM2 THEN BEGIN
            J2 ← J2 + 2 ;
            GO TO L1A ;
        ELSE END
        J1 ← J1 + 2 ;
        GO TO L1C ;
    END
END ;
DT[1],[30:17] ← K3 + DT[3],[25:8] ;
DT[2],[30:17] ← K4 + DT[5],[25:8] ;
WRITE (FIL2[N0], FMTC, N) ;
WRITE (SW01[IFIL+IF1], N, DT[*]) ;
OUT2 (DT, N+3, FIL2) ;
IF TM1 < TM2 THEN BEGIN
    N1 ← 0 ;
    J1 ← J2 ← 1 ;
    GO TO L1 ;
    N2 ← 0 ;
    J1 ← J2 ← 1 ;
    GO TO L1 ;
END ;
IF DT[2×I+3],[33:10] MOD 500=0 AND I≠498 THEN BEGIN
    DT[0],[18:30] ← DT[0],[18:30] + 1 ;
    IF DT[0],[18:30] = 1 THEN
        OUT2 (DT, N+3, FIL2) ;
        WRITE (SW01[IFIL+IF1], N, DT[*]) ;

```

```

        J1 ← I + J1 + 2
        J2 ← I + J2 + 2
        GO TO L1
        N ← N + 4
        END
L5:
    DT[0].[18:30] ← DT[0].[18:30] + 1
    DT[1].[30:17] ← K3 + DT[3].[25:8]
    DT[2].[30:17] ← K4 + DT[5].[25:8]
    IF DT[0].[18:30] = 1 THEN
        OUT2 (DT, N-3, FIL2)
        ELSE
            FOR I ← 0 STEP 1 UNTIL P1-1 DO
                IF DT[0].[18:30] MOD P = I THEN
                    OUT2 (DT, N-1, FIL2)
            WRITE (SW01[IFIL+IF1], N, DT[*])
            J1 := 500 + J1
            J2 := 500 + J2
            IF Z OR (DT[0].[18:30] ≤ M) THEN
                GO TO L1
L2:
        IFL1 := IFL1 + 1
        OUT2 (DT, 1002, FIL2)
        DT[0] ← 0
        IF IFL1 < IFL[IFIL] THEN BEGIN
            WRITE (FIL2[PAGE])
            GO TO LFIL
        END
        IFL1 ← 0
        LOCK (SW11[IFIL], RELEASE)
        LOCK (SW12[IFIL], RELEASE)
        IF IF1 = 0 THEN
            CLOSE (SW01[IFIL+IF1], *)
            ELSE
                REWIND (SW01[IFIL+IF1])
        WRITE (FIL2[PAGE])
        IFIL := IFIL + 1
        IF IFIL < IP THEN THEN
            GO TO LFIL
        RNTIM1 := (TIME(2) - RNTIM)/60
        WRITE (FIL2, FMTA, RNTIM1)
        WRITE (FIL2[PAGE])

```

```

REWIND (FILP1) ;
REWIND (SW01[IFIL+IF1-1]) ;
IFIL := 0 ;
LP5A:
L2B: N := WORD(SW01[IFIL], LBL) ;
IF LBL = 1 THEN GO TO L4 ELSE IF LBL = 2 THEN GO TO LP4 ;
READ (SW01[IFIL], N, DT[*]) ;
WRITE (FIL2, FMTB, FOR I:=2,100 DT[N-I]) ;
WRITE (FIL2[N0], FMTC, N) ;
OUT2 (DT, N-3, FIL2) ;
SPACE (SW01[IFIL], P-2)[L4] ;
L3: FOR I := 0 STEP 1 UNTIL P1-1 DO BEGIN
LP6A:
J1 ← DT[0].[12:6] ;
N := WORD (SW01[IFIL], LBL) ;
IF LBL = 1 THEN GO TO L4 ELSE IF LBL = 2 THEN GO TO LP6 ;
READ (SW01[IFIL], N, DT[*]) ;
IF DT[0].[12:6] ≠ J1 THEN BEGIN
SPACE (SW01[IFIL], "DT[0].[18:30]) ;
GO TO L2B END ;
IF (DT[0].[18:30] MOD P) ≠ 1 THEN BEGIN
SPACE(SW01[IFIL],P+1-(DT[0].[18:30] MOD P))[L4:LP6] ;
OUT2 (DT, N-1, FIL2) ;
GO TO LP6A END ;
WRITE (FIL2[N0], FMTC, N) ;
OUT2 (DT, N-1, FIL2) END ;
SPACE (SW01[IFIL], P-P1)[L4] ;
GO TO L3 ;
L4: RNTIM1 := (TIME(2) - RNTIM)/60 ;
WRITE (FIL2[PAGE], FMTA, RNTIM1) ;
IFIL := IFIL + 1 ;
IF IF1 = 0 THEN
IF IFIL < TP THEN
GO TO L2B ;
LOCK (SW01[IFIL], RELEASE) ;
GO TO LEND ;
L9: SPACE (SWI1[IFIL], 1)[L2:L9] ;

```

```

L8:  SPACE (SWI2[IFIL], 1)[L2:L8] ;
L10: SPACE (SWI2[IFIL], 1)[L2:L10] ;
L11: SPACE (SWI1[IFIL], 1)[L2:L11] ;
LP1: WRITE (FIL2[DBL], FP1, IFIL) ;
      RELEASE (SWI1[IFIL]) ;
      N1 := N2 := 0 ;
      WRITE (FILP1, FMTD, DT[0].[12:6], DT[0].[18:30], DT[1].[30:17],
              DT[2].[30:17]) ;
      IPAR := IPAR + 1 ;
      IF IPAR > 10 THEN GO TO LEND ;
      GO TO LP1A ;
LP2: WRITE (FIL2[DBL], FP2, IFIL) ;
      RELEASE (SWI2[IFIL]) ;
      N1 := N2 := 0 ;
      WRITE (FILP1, FMTD, DT[0].[12:6], DT[0].[18:30], DT[1].[30:17],
              DT[2].[30:17]) ;
      IPAR := IPAR + 1 ;
      IF IPAR > 10 THEN GO TO LEND ;
      GO TO LP1A ;
LP3: WRITE (FIL2[DBL], FP3, IFIL) ;
      RELEASE (SWI1[IFIL]) ;
      N1 := N2 := 0 ;
      J1 := J2 := 1 ;
      WRITE (FILP1, FMTD, DT[0].[12:6], DT[0].[18:30], DT[1].[30:17],
              DT[2].[30:17]) ;
      IPAR := IPAR + 1 ;
      IF IPAR > 10 THEN GO TO LEND ;
      GO TO LP3A ;
LP4: WRITE (FIL2[DBL], FP4, IFIL) ;
      RELEASE (SWI2[IFIL]) ;
      N1 := N2 := 0 ;
      J1 := J2 := 1 ;
      WRITE (FILP1, FMTD, DT[0].[12:6], DT[0].[18:30], DT[1].[30:17],
              DT[2].[30:17]) ;
      IPAR := IPAR + 1 ;
      IF IPAR > 10 THEN GO TO LEND ;
      GO TO LP3A ;

```

```

LP5:  WRITE (FIL2[DBL], FP5, IFIL)      ;
      RELEASE (SWD1[IFIL])              ;
      IPAR := IPAR + 1                   ;
      IF IPAR > 10 THEN GO TO LEND      ;
      GO TO LP5A                          ;
LP6:  WRITE (FIL2[DBL], FP6, IFIL)      ;
      RELEASE (SWD1[IFIL])              ;
      IPAR := IPAR + 1                   ;
      IF IPAR > 10 THEN GO TO LEND      ;
      GO TO LP6A                          ;
LEND:
BEGIN LABEL L1,L2                        ;
      FILE FILPN 0 (1,10)                ;
      ALPHA ARRAY A[0:9]                 ;
      REWIND (FILP1)                     ;
      WRITE (FIL2[PAGE])                 ;
L1:   READ (FILP1, 10, A[*])[L2]          ;
      WRITE (FILPN, 10, A[*])            ;
      WRITE (FIL2, 10, A[*])            ;
      GO TO L1                          ;
L2:   CLOSE (FILP1, PURGE)               ;
END                                       ;
END .

```

```

COMMENT -- FM DATA CONVERTER PROGRAM, PART 2, ADDITION OF WAVELENGTH ;
BEGIN INTEGER I,J,L,N,SN,FL,TPI,TPO,BLK,INTP,LBLK ;
      REAL TM, LAMBDA ;
      ARRAY T[0:10,0:50,0:4], LMB[0:4], STT,STP[0:25] ;
      ALPHA ARRAY A[0:10,2] ;
      INTEGER ARRAY SCAN[0:40] ;
      LABEL L1,L2,L3,L4,L5 ;
      BOOLEAN Z ;
      FILE IN FIL3 (5,10),
            TSI06 (1,1010),
            TSI07 (1,1010),
            TSI08 (1,1010),
            TSI09 (1,1010),
            TSI10 (1,1010) ;
      FILE FMDATA6 2 "FMDATA" "FILE6" (1, 1010, SAVE 365),
            FMDATA7 2 "FMDATA" "FILE7" (1, 1010, SAVE 365),
            FMDATA8 2 "FMDATA" "FILE8" (1, 1010, SAVE 365),
            FMDATA9 2 "FMDATA" "FILE9" (1, 1010, SAVE 365) ;
      SWITCH FILE SWIN + TSI06, TSI07, TSI08, TSI09, TSI10 ;
      SWITCH FILE SWOUT + FMDATA6, FMDATA7, FMDATA8, FMDATA9 ;
      FILE OUT FIL2 6 (5,15) ;
      FORMAT OUT FMT1 (2(I8, X8), I5),
            FMT2 (4(I4,".0"X1,I2,X1,I3,"."X1,I4,".0"X3),I4),
            FMT3 (I2," HOURS",I3," MINUTES",I3," SECONDS", X10,
            "TIME " I6) ;
      FORMAT OUT FMTA (4(I10,X10)) ;
      PROCEDURE OUT3 (A, N, F1) ;
        VALUE N ;
        INTEGER N ;
        ARRAY A[0] ;
        FILE F1 ;
      BEGIN INTEGER I,J,TM,T1,T2,T3 ;
        LIST LIST1 (T1,T2,T3,TM),
              LIST2 (FOR I + 3 STEP 4 UNTIL N=3 DO [FOR J + 0,1,2,3 DO [
        A[I+J],[1:13],A[I+J],[4:5], A[I+J],[25:8], A[I+J],[33:10], A[I+J],
        [14:11]], (I+1) DIV 4]) ;
        FOR I + 1,2 DO

```

BEGIN


```

        TM ← A[I].[30:17]
        T1 ← TM DIV 3600
        T2 ← (TM - 3600×T1) DIV 60
        T3 ← TM - 3600×T1 - 60×T2
        WRITE (F1, FMT3, LIST1)
    IF (N=3) MOD 4 ≠ 0 THEN
        FOR I ← N+1 STEP 1 WHILE (I+N-3) MOD 4 ≠ 0 DO
            A[I] ← 0
        WRITE (F1, FMT2, LIST2)
    END
    PROCEDURE WORD (FILEID, N, LEOF, LPAR)
        FILE FILEID
        INTEGER N
        LABEL LEOF, LPAR
    BEGIN STREAM PROCEDURE S (A,B)
        BEGIN
            SI ← A
            DI ← B
            SI ← SI - 8
            DS ← WDS
        END
        READ (FILEID[NO])[LEOF:LPAR]
        S (FILEID(0), N)
    END
    BEGIN INTEGER I,J,K
        LABEL L1,L2
        FORMAT IN FMT1 (5(F7.2,X3)),
            FMT2 (2(I4,X6)),
            FMT3 (X13,F9.3)
        LIST LIST1 (FOR I ← 0,1,2,3,4 DO LMB[I]),
            LIST2 (FOR K ← 0,1,2,3,4 DO T[I,J,K])
        READ (FIL3, FMT2, INTP, LBLK)
        READ (FIL3, FMT1, LIST1)
    L1: READ (FIL3, FMT2, J, J)[L2]
        READ (FIL3, FMT3, LIST2)
        GO TO L1
    L2: CLOSE (FIL3, RELEASE)
    END

```



```

FL ← -1
TPI ← TPO ← SN ← 0
L1: WORD (SWIN[TPI], N, L3, L1)
READ (SWIN[TPI], N, A[*])
BLK ← BLK + 1
IF A[0].[18:30] < 10 AND NOT Z THEN BEGIN
    IF FL ≠ -1 THEN
        SCAN[FL] ← SN
        SN ← L ← 0
        FL ← FL + 1
        IF FL MOD 5 = 0 AND FL ≠ 0 THEN BEGIN
            CLOSE (SWOUT[TPO], *)
            TPO ← TPO + 1
            STT[FL] ← A[1].[30:17]
            BLK ← 1
            Z ← TRUE
        END
    ELSE THEN
        IF A[0].[18:30] > 100
            Z ← FALSE
STP[FL] ← A[1].[30:17]
A[0].[6:12] ← N
A[0].[18:6] ← FL + 1
A[0].[24:12] ← SN + 1
A[0].[36:12] ← BLK
IF A[2].[30:17] < T[FL,SN,0] = 1.0 THEN BEGIN
    WRITE (SWOUT[TPO], N, A[*])
    GO TO L1
END
FOR I ← 4 STEP 4 UNTIL (IF BLK=1 THEN N=3 ELSE N=1) DO BEGIN
    TM ← A[2].[30:17] = A[3].[25:8] + A[I].[25:8] + A[I].[33:10]/
        1000
    IF TM < T[FL,SN,0] THEN
        GO TO L2
    IF T[FL,SN,L] ≠ T[FL,SN,L+1] THEN
        LAMBDA ← LMB[L] + (TM-T[FL,SN,L])×(LMB[L+1]-LMB[L])/
            (T[FL,SN,L+1]-T[FL,SN,L])
    FOR J ← -1,0,1,2 DO
        A[I+J].[1:13] ← ENTIER (LAMBDA+0.5)

```

```

        IF TM > T[FL,SN,L+1]                THEN BEGIN
            L ← L + 1                          ;
            IF L ≥ 4                            THEN BEGIN
                IF T[FL,SN+1,0] = 99999.999    THEN BEGIN
                    WHILE A[0].[18:30]>10 DO
                        READ (SWIN[TPI], 1, A[*])[L3:L1] ;
                        SPACE (SWIN[TPI], -1)          ;
                    GO TO L1                          END ;
                L ← 0                                ;
                SN ← SN + 1                          END ;
                                                    END ;
L2:                                     END ;
        IF BLK MOD LBLK = 0                    THEN
            OUT3 (A, N, FIL2)                    ;
            WRITE (SWOUT[TPO], N, A[*])           ;
            GO TO L1                              ;
L3:     SCAN[FL] ← SN                          ;
        A[0] ← 0                                ;
        REWIND (SWIN[TPI])                      ;
        TPI ← TPI + 1                          ;
        IF TPI < INTP                            THEN
            GO TO L1                              ;
        WRITE (FIL2[PAGE])                      ;
        FOR I ← 0 STEP 1 UNTIL FL DO
            WRITE (FIL2, FMT1, STT[I], STP[I], SCAN[I]) ;
END .

```

```

COMMENT == COMMUTATOR REDUCTION PROGRAM (NEW) ;
BEGIN INTEGER I,J,K,L,N,FIL,CNT1,CNT2,PAGE1,PAGE2,BLK ;
      INTEGER ARRAY M[0:28] ;
      REAL T1,T2,T3,SLOPE,V0,V1,V2 ;
      ALPHA ARRAY A[0:350] ;
      LABEL L1,L2,L3,L4 ;
      LABEL LP1 ;
      ARRAY B[0:28,0:950], C[0:28,0:40], D[0:150], P,T[0:30] ;
      FILE OUT  FIL3 6 (5,15) ;
              FIL4 6 (5,15) ;
      FILE IN   FDT1 "COMMUTR" "FDT1" (1,300),
              FDT2 "COMMUTR" "FDT2" (1,300),
              FDT3 "COMMUTR" "FDT3" (1,300) ;
      SWITCH FILE SWFIL + FDT1, FDT2, FDT3 ;
      FILE FDISK DISK SERIAL [1:800] (2,200) ;
      FORMAT OUT FMT1 (X43,"COMMUTATED DATA"/X40,"NATURAL SKY BACKGROUND"///,
              X13,"ANGLE IN DEGREES    SOL",X6,"PC  CLUTCH VOLTAGES",
              X12,"TEMPERATURE IN DEGREES F"/" TIME GMT    REL    SUN",
              "    SPT  AZ  MON    AZIMUTH DIFF ELEVATION DIFF    ",
              "    PC  FRM  MNB  TMB  ELB"///),
      FMT1A(X43,"COMMUTATED DATA"/X40,"NATURAL SKY BACKGROUND"///,
              X27,"VOLTAGES"/" TIME GMT    MAIN  ELCT  TM    REF",
              "    THERM    PC"///),
      FMT2 (X113,"PAGE",I2),
      FMT3 (X68,X10,5(I3,X2)),
      FMT4 (X27,I3,X3,F3.1,X2,2(F4.1,X1),I2,X3),
      FMT5 (I2,"8",I2,"",F4.1,X2,3(I4,X1)),
      FMT6 (I2,"8",I2,"",F4.1,X30,2(F4.1,X2)),
      FMT7 (X14,4(F4.1,X2)),
      FMT8 (X5,"NUMBER OF BLOCKS USED",I10) ;
      LIST LIST1 (T1,T2,T3,P[1],P[3],P[2]),
      LIST2 (FOR L + 4,5,6,8 DO P[L],T1,P[7],P[9],T2),
      LIST3 (FOR L + 12 STEP 1 UNTIL 16 DO P[L]),
      LIST4 (P[18],P[19],P[17],P[28]),
      LIST5 (T1,T2,T3,V1,V2) ;
      DEFINE FORJ = FOR J + 0 STEP 1 UNTIL # ;
      REAL PROCEDURE MIN(A,B);VALUE A,B;REAL A,B;MIN+IF A<B THEN A ELSE B ;

```

PROCEDURE REED (F, A, N, LEOF)	;
FILE F	;
ARRAY A[0]	;
INTEGER N	;
LABEL LEOF	;
BEGIN STREAM PROCEDURE S (A,B)	;
BEGIN SI ← A	;
DI ← B	;
SI ← SI - 8	;
DS ← WDS	;
END S	;
LABEL L1,L2,L3	;
L1: READ (F[NO])[LEOF:L2]	;
S(F(0), N)	;
READ (F, N, A[*])	;
GO TO L3	;
L2: RELEASE (F)	;
GO TO L1	;
L3:	
END REED	;
REAL PROCEDURE AVG (A,N)	;
VALUE N	;
ARRAY A[0]	;
INTEGER N	;
BEGIN INTEGER I,M	;
REAL T1,T2,AV,S	;
T1 ← T2 ← 0	;
FOR I ← 0 STEP 1 UNTIL N-1 DO	BEGIN
T1 ← T1 + A[I]	;
T2 ← T2 + A[I]*2	END
AV ← T1/N	;
S ← SQRT(T2/N - AV*2)	;
T1 ← T2 ← M ← 0	;
FOR I ← 0 STEP 1 UNTIL N-1 DO	
IF ABS(A[I]-AV) ≤ S	THEN BEGIN
M ← M + 1	;
T1 ← T1 + A[I]	;

```

        T2 ← T2 + A[I]*2                                END ;
    AVG ← T1/M                                           ;
END AVG                                                 ;
REAL PROCEDURE RES(X)      § VALUE X                    § REAL X      ;
BEGIN INTEGER I            § REAL T                    § ARRAY R,TP[0:32] ;
    FILL R[*] WITH 35.17, 42.11, 50.09, 61.14, 76.35, 94.82, 120.90,
        136.77, 156.06, 176.71, 202.11, 230.23, 261.22, 297.62,
        337.00, 374.42, 437.58, 469.81, 489.87, 514.29, 561.43,
        589.82, 635.10, 670.49, 730.00, 790.00, 855.00, 926.00,
        1000.0, 1080.0, 1160.0 ;
    FILL TP[*] WITH 130.0, 120.0, 110.0, 100.0, 90.0, 80.0, 70.0,
        65.0, 60.0, 55.0, 50.0, 45.0, 40.0, 35.0,
        30.0, 25.0, 20.5, 18.0, 16.5, 15.0, 12.5,
        11.0, 9.0, 7.5, 5.0, 2.5, 0.0, -2.5,
        -5.0, -7.5, -10.0 ;
    I ← -1 ;
    DO I ← I + 1 UNTIL (R[I] > X) OR (I > 31) ;
    IF I > 31
        THEN
        T ← 99999999.9
        ELSE
        IF I = 0
            THEN
            T ← (R[0] - X)*(TP[1] - TP[0])/(R[0] - R[1]) + TP[0]
            ELSE
            T ← (R[I] - X)*(TP[I] - TP[I-1])/(R[I] - R[I-1])
                +TP[I] ;
    RES ← T
        END RES ;
    FIL ← 2 ;
    SPACE (SWFIL[FIL], 1) ;
    CNT1 ← CNT2 ← BLK ← 0 ;
    PAGE1 ← PAGE2 ← 1 ;
    WRITE (FIL3, FMT2, PAGE1) ;
    WRITE (FIL4, FMT2, PAGE2) ;
    WRITE (FIL3, FMT1) ;
    WRITE (FIL4, FMT1A) ;
WHILE TRUE DO BEGIN
    IF BLK ≥ 500 THEN GO TO L4 ;
    FOR I ← 0 STEP 1 UNTIL 28 DO
        M[I] ← -1 ;

```

```

L1: REED (SWFIL[FIL], A, N, L4) ;
    BLK ← BLK + 1 ;
    A[0] ← N ;
    FOR I ← 3 STEP 1 UNTIL N-1 DO
        IF A[I].[43:5] = 1 THEN BEGIN
            B[1,M[1]←M[1]+1] ← A[I].[14:11] ;
            B[0,M[0]←M[0]+1] ← A[I].[30:17]-A[3].[25:8]+A[I].[25:8]
                                +A[I].[33:10]/1000 END ;
        WRITE (FDISK, N, A[*]) ;
        IF M[1] ≤ 760 THEN ;
            GO TO L1 ;
        REWIND (FDISK) ;
    FOR J ← 2 STEP 1 UNTIL 25, 27, 28 DO BEGIN
L2: READ (FDISK[N], 1, A[*])[L3] ;
        N ← A[0] ;
        READ (FDISK, N, A[*]) ;
        FOR I ← 3 STEP 1 UNTIL N-1 DO
            IF A[I].[43:5] = J THEN
                B[J,M[J]←M[J]+1] ← A[I].[14:11] ;
            GO TO L2 ;
L3: REWIND (FDISK) END ;
    FOR I ← 1, 2, 25, 27 DO
        D[I] ← AVG(B[I,*], M[I]) ;
    SLOPE ← 4.0/(D[1]-D[2]) ;
    V0 ← D[2] - 1.0/SLOPE ;
    V1 ← (D[27] - V0)*SLOPE*3.84 ;
    V2 ← (D[25] - V0)*SLOPE*3.93 ;
    FOR I ← 0 STEP 25 UNTIL MIN(M[5], M[24]) DO BEGIN
        K ← I DIV 25 ;
        FORJ 24 DO D[J] ← (B[5,I+J] - V0)*SLOPE ;
        FORJ 24 DO D[J+25] ← (B[24,I+J] - V0)*SLOPE ;
        C[5,K] ← AVG(D, 50) END ;
    FOR I ← 0 STEP 75 UNTIL MIN(M[3], M[10]) DO BEGIN
        K ← I DIV 75 ;
        FORJ 74 DO D[J] ← (B[3,I+J] - V0)*SLOPE ;
        FORJ 74 DO D[J+75] ← (B[10,I+J] - V0)*SLOPE ;
        C[3,K] ← AVG(D, 150) END ;

```



```

FOR I = 0 STEP 75 UNTIL M[4]-75 DO                                BEGIN
    K = I DIV 75                                                ;
    FORJ 74 DO D[J] = (B[4,I+J] - V0)*SLOPE                      ;
    C[4,K] = AVG(D, 75)                                          ;
FOR L = 6,7,8,9 DO                                              END ;
FOR I = 0 STEP 75 UNTIL MIN(M[L], M[L+14]) DO                    BEGIN
    K = I DIV 75                                                ;
    FORJ 74 DO D[J] = (B[L,I+J] - V0)*SLOPE                      ;
    FORJ 74 DO D[J+75] = (B[L+14,I+J] - V0)*SLOPE                ;
    C[L,K] = AVG(D, 150)                                         ;
FOR L = 17, 18, 19, 28 DO                                      END ;
    FOR I = 0 STEP 150 UNTIL M[L] DO                               BEGIN
        K = I DIV 150                                           ;
        FOR J = 0 STEP 1 UNTIL 149 DO                             ;
            D[J] = (B[L,I+J] - V0)*SLOPE                          ;
            C[L,K] = AVG(D, 150)                                   ;
        END ;
FOR L = 10 STEP 1 UNTIL 16 DO                                    BEGIN
    FOR I = 0 STEP 1 UNTIL M[L] DO                                ;
        B[L,I] = (B[L,I] - V0)*SLOPE                              ;
        C[L,1] = AVG(B[L,*], M[L])                                ;
    END ;
FOR I = 0 STEP 1 UNTIL 29 DO                                     ;
    T[I] = B[0,I*25]                                              ;
FOR L = 11,13,14,15,16 DO                                       ;
    P[L] = RES(11500*C[L,1]/(V1-C[L,1]) - 665)                    ;
P[10] = RES(4957.7*C[10,1]/(23.01 - C[10,1]) - 185.5)          ;
P[12] = RES(8431.6*C[12,1]/(V2 - C[12,1]) - 484.9)              ;
WRITE (FIL3[NO], FMT3, LIST3)                                    ;
FOR I = 0 STEP 1 UNTIL 4 DO                                       BEGIN
    P[17] = 2.385*C[17,I]                                         ;
    P[18] = 8.031*C[18,I]                                         ;
    P[19] = 6.969*C[19,I]                                         ;
    P[28] = C[28,I]                                                ;
    WRITE (FIL4[NO], FMT7, LIST4)                                  ;
    FOR J = 2*I, 2*I+1 DO                                          BEGIN
        P[5] = C[3,J]                                             ;
        FOR L = 6,7,8,9 DO                                         ;
            P[L] = C[L,J]                                          ;

```

```

P[4] ← IF C[4,J] > 3.58 THEN 681.11 - C[4,J]×89.46 ELSE
      IF C[4,J] > 1.0 THEN 213.89 - C[4,J]×47.81 ELSE 225.0;
T1 ← 200×ABS(P[6] - P[8])/(P[6] + P[8]) ;
T2 ← 200×ABS(P[7] - P[9])/(P[7] + P[9]) ;
WRITE (FIL3[N0], FMT4, LIST2) ;
T1 ← T[K] DIV 3600 ;
T2 ← (T[K] - T1×3600) DIV 60 ;
T3 ← T[K] - 3600×T1 - 60×T2 ;
WRITE (FIL4, FMT6, LIST5) ;
CNT2 ← CNT2 +1 ;
IF CNT2 > 50 THEN BEGIN ;
      CNT2 ← 0 ;
      PAGE2 ← PAGE2 +1 ;
      WRITE (FIL4[PAGE2]) ;
      WRITE (FIL4, FMT2, PAGE2) ;
      WRITE (FIL4, FMT1A) ;
      END ;
FOR K ← 3×J, 3×J+1, 3×J+2 DO BEGIN ;
      P[2] ← (-90.0 + (T[K] - 25200)/240)/57.29578 ;
      P[2] ← COS(P[2]) - 0.070 ;
      IF P[2] ≠ 1.0 THEN ;
          P[3] ← 1.570796 - ARCTAN(P[2]/SQRT(1-P[2]×2)) ;
          ELSE ;
          P[3] ← 1.570796 ;
      P[3] ← P[3]×57.29578 ;
      C[5,K] ← C[5,K]×28.5/P[18] ;
      IF C[5,K] < 1.32 THEN ;
          C[5,K] ← 1.32 ;
      P[2] ← 62.44×(C[5,K] - 4.873 + 0.011×P[3]) ;
      IF P[2] < -20.0 THEN ;
          P[2] ← P[2] + 265.8 ;
      P[1] ← P[2] - P[3] ;
      T1 ← T[K] DIV 3600 ;
      T2 ← (T[K] - T1×3600) DIV 60 ;
      T3 ← T[K] - 3600×T1 - 60×T2 ;
      WRITE (FIL3, FMT5, LIST1) ;
      CNT1 ← CNT1 +1 ;
      IF CNT1 > 51 THEN BEGIN ;

```



```

        CNT1 ← 0 ;
        PAGE1 ← PAGE1 + 1 ;
        WRITE (FIL3[PAGE1]) ;
        WRITE (FIL3, FMT2, PAGE1) ;
        WRITE (FIL3, FMT1) ;
        END ;
        END ;
        END END ;
END ;
L4:  WRITE (FIL3[PAGE1]) ;
      WRITE (FIL3, FMT8, BLK) ;
END.

```

```

COMMENT DATA REDUCTION PROGRAM FOR OBTAINING INTENSITY DATA AND
POLARIZATION DATA AT A GIVEN TIME. THE PROGRAM WILL OBTAIN
ABSOLUTE INTENSITIES IF THE REFERENCE GENERATOR WAS
OPERATING PROPERLY, BUT IT WILL ALSO FURNISH RELATIVE
INTENSITIES IF THE GENERATOR AND QUARTER WAVE PLATE DRIVE HAS
STOPPED. INPUT DATA MUST BE IN THE FOLLOWING FORMAT:
CARD 1 COLUMN 1-5 STARTING TIME
COLUMN 11-15 STOPPING TIME
COLUMN 21-24 WAVELENGTH INTERVAL FOR SAMPLES
CARD 2 COLUMN 1-5 MIN. VALUE FOR "SHUTTER"
COLUMN 11-15 MAX. VALUE FOR "SHUTTER"
COLUMN 21-26 541F SHUTTER ATTENUATION (REAL)
COLUMN 31-36 541A SHUTTER ATTENUATION (REAL)
COLUMN 41-46 APPROX. GENERATOR FREQUENCY
CARD 3 COLUMN 1-7 541F GEN. PHASE ANGLE (REAL)
COLUMN 11-17 541A GEN. PHASE ANGLE (REAL)
COLUMN 21-24 MINIMUM WAVELENGTH FOR 541A TUBE
COLUMN 26-29 MAXIMUM WAVELENGTH FOR 541F TUBE
COLUMN 31-33 COMPUTE OPTION FOR GEN. DATA
COLUMN 34-36 COMPUTE OPTION FOR PM DATA
COLUMN 37-41 PRINT OPTION FOR GEN. DATA
COLUMN 42-46 PRINT OPTION FOR PM DATA ;
BEGIN INTEGER INTV, STRTJM, STPTM, N ;
FILE OUT FIL2 6 (5, 15),
FPUNCH 0 (5, 15) ;
DEFINE HETIME = (A[1],[30:17] + A[2],[30:17])/2 # ;
FORMAT OUT FMT1 ("MALFUNCTION OF AC GENERATOR"/"ONLY RELATIVE",
" INTENSITIES ARE OBTAINED"),
FMT2 (X1, I4),
FMT3 (X8, E10.3, X13, 2(F4.2, X8), F5.1),
FMT4 (X19, E10.3, 2(X8, F4.2), X9, F5.1),
FMT5 (X72, 2(R9.2, X13)),
FMT6 (X70, 2(X13, R9.2)),
FMT7 ("PROCESSOR TIME ", F6.1, " SECONDS"/"IN-OUT TIME ",
F6.1, " SECONDS"),
FMT8 (X47, "NATURAL SKY UV BACKGROUNDS"/X53,
"INTENSITY DATA"/X48, "ALTITUDE: ", I3, " ", I1,

```

```

"00 FEET"/X41, "STARTING SCATTER ANGLE: ", F5.1,
" DEGREES"/X41, "STOPPING SCATTER ANGLE: ", F5.1,
" DEGREES", X17,
"AMB TEMP (F) ", I3/X93, "AVG. SOL. MON. ", F3.1/
X87, "AVG. AZ. POS. (DEG.) ", I3//X14, "INTENSITY", X8,
"DEGREE OF", X16, "ANGLE OF", X11, "RELATIVE",
X14, "STANDARD"/X13, "UW/SQ.CM./NM", X5,
"POLARIZATION ELLIPTICITY POLARIZATION", X9,
"INTENSITY", X13, "DEVIATION"/"LAMBOA", X5, "541F",
X7, "541A ", 2(X2, "541F 541A"),
" 541F 541A", 2(X7, "541F", X7, "541A")///),
FMT9 ("STARTING TIME ", I2, ":", I2, ":", I2/"STOPPING TIME ", I2,
":", I2, ":", I2/"MINIMUM WAVELENGTH ", I5/"MAXIMUM WA",
"VELENGTH ", I5/I4, " INTERVALS OF ", I3, " ANGSTROMS"/),
FMT10(" PARITY ERROR == STEP 1"),
FMT11(" PARITY ERROR == STEP 2"),
FMT12(" PARITY ERROR == STEP 3"),
FMT14(" PARITY ERROR == STEP 5"),
FMT15("NO MINIMUM AND/OR MAXIMUM FOUND"/"MIN = 2000"/"MAX = ",
" 4000"),
FMT16("END OF FILE == START TIME NOT FOUND"),
FMT17("C[" , I2, " ] = " , R10.3, X5, F10.6),
FMT18("FINAL APPROXIMATION FOR FREQUENCY OF AC",
" GENERATOR WAS " , R12.5),
FMT19("PHASE ANGLE: " , F8.4/7(X25, "A[" , I1, " ] " , F10.5/)/),
FMT20("PHASE ANGLE: " , F8.4/"AMPLITUDE: " , F8.4/
3(X25, "A[" , I1, " ] " , F10.5/)/),
FMT21(10(F8.5, X3)),
FMT22("TUBE: " , I2/5(X10, "A[" , I1, " ] " , E12.5/)/),
FMT23("RUN DATE " , I2, "/" , I2, "/" , I2),
FMT24("RUN TIME " , I2, ":", I2, ":", I2),
FMT25("STANDARD DEVIATION " , R12.5/X3, 2(R12.5, X6), X2, I3),
FMT26(3(3(F10.5, X3))),
FMT27 (I4, X1, 2(F8.4, X2, F4.2, X2, 2(F5.3, X2))) ;
FORMAT IN FMTI1 (2(I5, X5), I4/2(I5, X5), 2(F6.2, X4), F6.3),
FMTI2(2(F7.4, X3), 2(I4, X1), 2I3, 2L5),
FMTI3 (2(F7.4, X3), F7.5) ;

```

```

REAL PI, PI2
REAL PROCEDURE ARCCOS (X)
VALUE X
REAL X
IF ABS(X) = 1.0 THEN
    ARCCOS ← 1.57079633×SIGN(X) ELSE
    ARCCOS ← 1.57079633 - ARCTAN(X/SQRT(1.0-X*2))
COMMENT ARC TANGENT PROCEDURE WHOSE OUTPUT IS BETWEEN 0 AND 2×PI
REAL PROCEDURE ATAN (A, B)
VALUE A, B
REAL A, B
BEGIN REAL T
IF B = 0 THEN
    T ← 1.57079633×SIGN(A) ELSE
    IF B < 0 THEN
        T ← 3.14159266 + ARCTAN(A/B) ELSE
        T ← ARCTAN (A/B)
IF T < 0 THEN
    ATAN ← T + 6.28318554 ELSE
    ATAN ← T
END ATAN
PROCEDURE DATE (FILEID)
FILE FILEID
BEGIN ALPHA D
INTEGER I, J, K
LABEL L1
INTEGER ARRAY MO[1:12]
D ← TIME(0)
FILL MO[*] WITH 31, 28, 31, 30, 31, 30, 31, 31, 30, 31, 30, 31
K ← 10×D.[18:6] + D.[24:6]
J ← 100×D.[30:6] + 10×D.[36:6] + D.[42:6]
IF J > (IF K MOD 4 = 0 THEN 366 ELSE 365) THEN
    GO TO L1
I ← 0
FOR I ← I + 1 WHILE J > 0 DO
    J ← J - MO[I]
    IF K MOD 4 = 0 AND I = 2 THEN

```

BEGIN

```

        J ← J - 1                                END ;
I ← I - 1                                        ;
J ← J + MO[I]                                    ;
WRITE (FILEID, FMT23, I, J, K)                  ;
L1: K ← TIME(1) DIV 60                            ;
I ← K DIV 3600                                    ;
J ← (K - I×3600) DIV 60                          ;
K ← K - I×3600 - J×60                            ;
WRITE (FILEID, FMT24, I, J, K)                  ;
END                                              ;
COMMENT CURVEFITTING PROCEDURE == EXPLANATION OF OPTIONS
        OPTION #1    STRAIGHT CURVEFITTING
        #2    STRAIGHT CURVEFITTING WITH STD. DEV. PRINTED
        #3    SAME AS #2 BUT WITH INPUT DATA LISTED
        #4    CURVEFITTING AND REJECTION OF DATA POINTS
                LYING OUTSIDE T STD. DEVIATIONS. THE STD. DEV.
                IS CALCULATED AND PRINTED
        #5    SAME AS 4 BUT WITH INPUT DATA LISTED
        #6    SAME AS #3 BUT WITH NO LISTING
        #7    SAME AS #5 BUT WITH NO LISTING
PROCEDURE COMPUTE (N, M, X, T, A, E, D, FILEID)
        VALUE N, M, T, D
        FILE FILEID
        INTEGER N, M, D
        ARRAY X[0:M-1], A[0]
        INTEGER ARRAY E[0]
        REAL T
BEGIN
        INTEGER I, J, K, L, P
        REAL T1, T2, S, D
        BOOLEAN ZZ
        LABEL L1, L2
        ARRAY Z[0:M-1, 0:M], B, C[0:N-1]
        LIST LIST1 (S, T1, T2, P),
                LIST2 (FOR I←0 STEP 1 UNTIL P-1 DO [X[M, I], B[I], C[I]])
        ZZ ← FALSE
        E[0] ← P ← N
        FOR I ← 1 STEP 1 UNTIL N DO

```

```
THEN BEGIN ;  
      END ;  
THEN  
      BEGIN ;  
          ;  
      END ;  
          ;  
      BEGIN ;  
          ;  
      END END ;  
THEN  
          ;  
              BEGIN ;  
                  ;  
                  ;  
                  ;  
              END ;  
                  ;  
                  ;
```



```

IF O > 3 AND O < 6 THEN
    WRITE (FILEID, FMT26, LIST2) ;
IF O < 6 THEN
    WRITE (FILEID, FMT25, LIST1) ;
IF O = 3 OR O = 5 OR O = 7 THEN BEGIN
    IF ZZ THEN
        GO TO L2 ;
    ZZ = TRUE ;
    P = 0 ;
    FOR I = 0 STEP 1 UNTIL N-1 DO
        IF ABS(C[I]) < T*S THEN BEGIN
            FOR J = 0 STEP 1 UNTIL M DO
                X[J,P] = X[J,I] ;
            E[P+1] = I ;
            P = P + 1 ;
        END ;
    E[0] = P ;
    GO TO L1 ;
L2:END COMPUTE ;
DATE (FIL2) ;
PI = 3.1415926536 ;
PI2 = 1.5707963268 ;
BEGIN INTEGER I, SCAN, TEMP, AZPOS ;
FILE FDISK1 DISK SERIAL [1:1010] (1, 5, 30),
    FDISK2 DISK SERIAL [1:600] (1, 2, 30),
    FDISK3 DISK RANDOM [1:6000] (1, 3, 30) ;
FILE IN FIL1 (2, 10),
    FMDATA (1, 1023),
    ALTTEMP "CLPNTS" "ALTTEMP" (1, 1010, 8),
    CONSTS "CLPNTS" "CONSTS" (1, 1010, 8),
    PMAMP "CLPNTS" "PMAMP" (1, 1001) ;
FILE OUT FTAPE 2 (3, 1023, INTV*6, SAVE 5),
    FTP1 2 (2, 920, 9, SAVE 2) ;
ARRAY SHUT, ZETA, ETA[0:1], B, C1[0:8], TM[0:1, 0:3+(STPTM-STRTM)
    DIV 20] ;
INTEGER ARRAY OPT[0:2] ;
BOOLEAN ARRAY TEST[0:1] ;
REAL LAMBDAA, LAMBDAA1, SHUT0, SHUT1, DMGA,

```



```

        LMB1, LMB2, ANG1, ANG2, STER, SOLMON
        LABEL L1, L2, L3
        SWITCH FILE SWFIL < CONSTS, ALTTEMP
LIST LIST1 (STRITM, STPTM, INTV, SHUT0, SHUT1, SHUT[0], SHUT[1], OMGA),
LIST2 (ZETA[0], ZETA[1], LMB1, LMB2, OPT[0], OPT[1],
        TEST[0], TEST[1]),
LIST3 (ETA[0], ETA[1], STER)
PROCEDURE REED (F, N, A, LE, LP)
        FILE F
        INTEGER N
        ARRAY A[0]
        LABEL LE, LP
BEGIN READ (FIND), 1, A[*]][LE:LP]
        N < A[0], [6:12]
        READ (F, N, A[*])
END
        READ (FIL1, FMTI1, LIST1)
        READ (FIL1, FMTI2, LIST2)
        READ (FIL1, FMTI3, LIST3)
        FOR I < 0, 1 DO
                READ (SWFIL[I], 8, B[*])
COMMENT      INITIALIZATION BLOCK WHERE ALL CONSTANTS TO BE USED BY THE
                PROGRAM ARE PLACED ON THE DISK FROM TAPE, FROM WHICH THEY
                WILL EVENTUALLY BE READ
BEGIN INTEGER J, K
        ARRAY C[0:4]
        IF I = 0
                THEN BEGIN
                        C1[0] < C1[2] < B[6]
                        C1[1] < C1[3] < B[7]
                        C1[4] < B[2]/2
                        FOR J < 0 STEP 1 UNTIL B[2]-1 DO
                                READ (CONSTS, 5, C[*])
                                WRITE (FDISK1, 5, C[*])
                                REWIND (CONSTS)
                                REWIND (FDISK1)
                                C1[5] < B[4]
                                ELSE BEGIN

```

```

        C1[6] ← B[5]
        FOR J ← 0 STEP 1 UNTIL B[2]-1 DO
            READ (ALTTEMP, 2, C[*])
            WRITE (FDISK2, 2, C[*])
        REWIND (ALTTEMP)
        REWIND (FDISK2)
END *

C1[7] ← 42120
C1[8] ← 5
CLOSE (FIL1, RELEASE)
BEGIN INTEGER I,J,K,L,M,N,P,R
REAL A1,B1,S,OMEGA,OMIN,OMAX
ARRAY G[0:250], GEN,LMB[0:6×INTV], PM[0:1,0:6×INTV], C[0:21],
        PMCAL[0:1,0:1001]
ALPHA ARRAY A[0:1022]
LIST LIST1 (FOR A1 ← STRTTM, STPTM DO [I ← A1 DIV 3600, J ← (A1 -
        3600×I) DIV 60, A1 = 3600×I + 60×J], LAMBD A0,LAMBD A1,
        M, INTV)
BOOLEAN Z
LABEL L1,L2,L3,L4,L6,L7,L8,L9,L10,LE1,LE2,LP1,LP2,LP3,LP5
READ (PMAMP, 8, A[*])
FOR I ← 0,1 DO
    READ (PMAMP, 1001, PMCAL[I,*])
L ← 0
Z ← FALSE
LAMBD A0 ← 1
LAMBD A1 ← 0
COMMENT DETERMINATION OF MINIMUM AND MAXIMUM WAVE LENGTH
DO READ (FM DATA, 4, A[*])[LE1:LP1] UNTIL A[3].[1:13] = 0
DO READ (FM DATA, 4, A[*])[LE1:LP1] UNTIL A[3].[1:13] ≠ 0
SPACE (FM DATA, -2)
REED (FM DATA, N, A, LE1, LP1)
FOR I ← 7 STEP 4 UNTIL N-1 DO
    IF A[I-4].[1:13] = 0 AND A[I].[1:13] ≠ 0 THEN
        LAMBD A0 ← A[I].[1:13]
        GO TO L1

```

```

L1:  DO READ (FM DATA, 4, A[*])[LE2:LP2] UNTIL A[3],[1:13] = 0      ;
    SPACE (FM DATA, -2)                                           ;
    REED (FM DATA, N, A, LE1, LP1)                                ;
    FOR I + 7 STEP 4 UNTIL N=1 DO
        IF A[I-4],[1:13] ≠ 0 AND A[I],[1:13] = 0 THEN BEGIN
            LAMBDA1 ← A[I-4],[1:13]
            GO TO L2
        END ;
L2:  P ← (N-3) DIV 4 - 1
    FOR I ← 0 STEP 1 UNTIL P DO
        G[I] ← A[4×I+3],[14:11]
    REWIND (FM DATA)
    M ← (LAMBDA1 - LAMBDA0)/INTV
    WRITE (FIL2, FMT9, LIST1)
COMMENT POSITIONING OF TAPE TO STARTING TIME
L3:  READ (FM DATA, 3, A[*])[LE2:LP2]
    IF A[1],[30:17] ≠ A[2],[30:17] OR (A[1],[30:17] < STRTTM)
        THEN
            GO TO L3
    SPACE (FM DATA, -1)
    SCAN ← 0
COMMENT FILLING OF SCRATCH TAPE WITH DATA TO BE USED IN THE
    CALCULATIONS
L4:  REED (FM DATA, N, A, L8, LP3)
    K ← 3
    IF A[3],[1:13] ≠ 0 THEN BEGIN
        TM[0, SCAN] ← HOTIME
        J ← (A[3],[1:13] - LAMBDA0) DIV INTV
        ELSE
            BEGIN
                J ← 0
                IF A[N-1],[1:13] ≠ 0 THEN BEGIN
                    DO K ← K+4 UNTIL A[K],[1:13] ≠ 0
                    TM[0, SCAN] ← HOTIME
                    IF A[N-1],[1:13] = 0 THEN
                        END
                END
            END
    END ;
L6:  FOR I ← K STEP 4 UNTIL N=1 DO
    L ← L+1
    LMB[L] ← A[I+1],[1:13]

```

```

GEN[L] ← A[I].[14:11]
PM[0,L] ← PMCAL[0,A[I+2].[14:11]/2]
PM[1,L] ← PMCAL[0,A[I+3].[14:11]/2]
IF A[I+1].[14:11] > SHUT0 AND A[I+1].[14:11] < SHUT1
    THEN
        FOR R ← 0,1 DO
            PM[R,L] ← PM[R,L] × SHUT[R]
        IF A[I].[1:13] = 0 OR (A[I].[1:13] = LAMBDA0) DIV INTV > J
            THEN BEGIN
                J ← J+1
                GEN[0] ← PM[0,0] ← PM[1,0] ← LMB[0] ← L+1
                WRITE (FTAPE, L+1, LMB[*])
                WRITE (FTAPE, L+1, GEN[*])
                WRITE (FTAPE, L+1, PM[0,*])
                WRITE (FTAPE, L+1, PM[1,*])
                L ← 0
COMMENT      DETERMINATION OF END OF SCAN CONDITIONS
                IF A[I].[1:13] = 0
                    THEN BEGIN
                        TM[1, SCAN] ← HOTIME
                        SCAN ← SCAN + 1
                        GO TO L4
                    END
                IF J > M
                    THEN
                        J ← 0
                        END
                        END
L7: REED (FMDATA, N, A, L8, LP5)
    K ← 3
        IF (A[1].[30:17] = A[2].[30:17]) AND (A[1].[30:17] < STPTM)
            THEN
                GO TO L6
                TM[1, SCAN] ← HOTIME
L8: REWIND (FTAPE)
    LOCK (FMDATA, RELEASE)
COMMENT      CALCULATION OF APPROXIMATE FREQUENCY OF REF. GEN.
    OMIN ← 0.9 × OMGA
    OMAX ← 1.1 × OMGA
    S ← (OMAX - OMIN) / 10.0
L9: K ← 0
    FOR OMGA ← OMIN STEP S UNTIL OMAX DO
        BEGIN

```

III
(3)

```

SCAN ← 0
L1: SPACE (FTAPE, 4)[L2]
READ (FTAPE[NO], *, N)[L2]
BEGIN INTEGER I, J, K, Q
REAL PHI, AMP, R, OMGA, A1, B1, LAMBDA, BETA2, INT, POL, ELL, PHI2
INTEGER ARRAY B, C[0:N+INTV]
ARRAY GEN[0:N+INTV], PM[0:1, 0:N+INTV], A[0:7], X[0:7, 0:N+INTV],
      THETA2[0:N+INTV], LMB[0:N+INTV], TAPE[0:9]
LABEL L1, L2, L3, L4
LIST LIST1 (PHI, FOR I ← 0 STEP 1 UNTIL 6 DO [I, A[I]]),
      LIST2 (PHI, AMP, FOR I ← 0, 1, 2 DO [I, A[I]]),
      LIST3 (FOR I ← 0 STEP 1 UNTIL N-2 DO THETA2[I]),
      LIST4 (Q, FOR I ← 0 STEP 1 UNTIL 4 DO [I, A[I]])
LAMBDA ← 999999
L1: READ (FTAPE[NO], *, N)[L4]
READ (FTAPE, N, LMB[*])
READ (FTAPE, N, GEN[*])
FOR I ← 0, 1 DO
  READ (FTAPE, N, PM[I, *])
COMMENT DETERMINATION OF THE ANGLE OF THE QUARTER WAVE PLATE
FOR I ← 1 STEP 1 UNTIL N-1 DO
  X[0, I-1] ← 1.0
  X[1, I-1] ← SIN(OMGA×(I))
  X[2, I-1] ← COS(OMGA×(I))
  FOR K ← 1, 2 DO
    X[2×K+1, I-1] ← X[1, I-1]×((I)×K)
    X[2×K+2, I-1] ← X[2, I-1]×((I)×K)
  X[7, I-1] ← GEN[I]
COMPUTE (N-2, 7, X, 1.0, A, B, OPT[0], FIL2)
PHI ← ATAN (A[2], A[1])
IF TEST[0] THEN
  WRITE (FIL2, FMT19, LIST1)
IF ABS (A[4]-A[3]) > 0.001 THEN
  IF ABS (A[2]) > ABS (A[1]) THEN
    OMGA ← OMGA - A[3]/A[2]
  ELSE
    OMGA ← OMGA + A[4]/A[1]
FOR I ← 0 STEP 1 UNTIL B[0]-1 DO

```

```

        X[1,I] + SIN(OMGA*B[I+2])
        X[2,I] + COS(OMGA*B[I+2])
        X[3,I] + GEN[B[I+2]]
COMPUTE (B[0], 3, X, 1.0, A, C, OPT[0], FIL2)
PHI + ATAN (A[2], A[1])
AMP + SQRT (A[1]*2 + A[2]*2)
IF TEST[0] THEN
    WRITE (FIL2, FMT20, LIST2)
IF AMP < 250.0 THEN BEGIN
    WRITE (FIL2, FMT1)
    GO TO L2
FOR I + 0 STEP 1 UNTIL N-2 DO
    THETA2[I] + PHI + I*OMGA
IF TEST[0] THEN
    WRITE (FIL2, FMT21, LIST3)
A1 + 0
FOR I + 1 STEP 1 UNTIL N-1 DO
    A1 + A1 + LMB[I]
A1 + A1/(N-1)
IF LAMBDA > A1 THEN BEGIN
    WRITE (FIL2[PAGE])
    SCAN + SCAN + 1
    FOR I + 0,1 DO BEGIN
        J + (TM[I,SCAN] - C1[7])/C1[8]
        I + ((TM[0,SCAN]+TM[1,SCAN])/2 - C1[5])/C1[6]
        READ (FDISK2[I], 2, A[*])
        I + ENTIER (A[0])
        J + (A[0] - I)*10
        IF J = 10 THEN BEGIN
            J + 0
            I + I + 1
            END
        WRITE (FIL2, FMT8, I, J, ANG1, ANG2, A[1], SOLMON, AZPOS)
        END
    END
LAMBDA + A1
WRITE (FIL2[NO], FMT2, LAMBDA)
IF OPT[1] < 6 THEN
    WRITE (FIL2[DBL1])

```



```

FOR Q ← 0 STEP 1 UNTIL 1 DO                                BEGIN
  IF LAMBDA > LMB2                                          THEN
    Q ← 1                                                  ;
COMMENT CURVEFITTING THE PM CURRENT TO OBTAIN ITS FOURIER COMPONENTS;
FOR I ← 1 STEP 1 UNTIL N-1 DO                              BEGIN
  BETA2 ← 2×ZETA[Q] + THETA2[I-1]                          ;
  X[0,I-1] ← 1.0                                           ;
  X[1,I-1] ← SIN(BETA2)                                     ;
  X[2,I-1] ← COS(BETA2)                                     ;
  X[3,I-1] ← SIN(2×BETA2)                                   ;
  X[4,I-1] ← COS(2×BETA2)                                   ;
  X[5,I-1] ← PM[Q,I]                                       ;
  COMPUTE (N-1, 5, X, 0.9, A, B, OPT[1], FIL2)             ;
  IF TEST[1]                                                THEN
    WRITE (FIL2, FMT2, LIST4)                               ;
  IF Q = 0                                                  THEN
    I ← (LAMBDA - C1[0])/C1[1]                               ELSE
    I ← (LAMBDA - C1[2])/C1[3] + C1[4]                      ;
  READ (FDISK1[I], 5, GEN[*])                               ;
  INT ← A[0]×GEN[0] + A[4]×GEN[1]                           ;
  POL ← GEN [2]×SQRT(A[4]*2 + A[3]*2)/INT                   ;
  PHI2 ← ATAN (A[3], A[4])                                   ;
  ELL ← A[2]×GEN[3]/INT + GEN[4]×POL×SIN(PHI2)             ;
  IF INT < 0                                                THEN
    INT ← 0                                                  ELSE
    INT ← INT/STER                                           ;
  PHI2 ← PHI2/2 + ETA[Q]                                     ;
  TAPE[0] ← LAMBDA                                          ;
  TAPE[4×Q+1] ← IF INT > 0 THEN LN(INT) ELSE 0              ;
  TAPE[4×Q+2] ← POL                                          ;
  TAPE[4×Q+3] ← ELL                                          ;
  TAPE[4×Q+4] ← PHI2                                        ;
  IF Q = 0                                                  THEN
    WRITE (FIL2[N0], FMT3, INT,POL,ELL,PHI2)               ELSE
    WRITE (FIL2[N0], FMT4, INT,POL,ELL,PHI2)               ;
  IF OPT[1] < 6                                             THEN

```

```

        WRITE (FIL2[DBL])
        IF LAMBDA < LMB1
            Q ← 1
            THEN
                END
        GO TO L3
COMMENT -- AVERAGING PORTION FOR WHEN THE AC GENERATOR IS NOT
FUNCTIONING
L2:  WRITE (FIL2[NO], FMT2, LAMBDA)
    FOR Q ← 0 STEP 1 UNTIL 1 DO
        IF LAMBDA < LMB2
            THEN
                BEGIN
                    Q ← 1
                    A1 ← B1 ← 0
                    FOR I ← 1 STEP 1 UNTIL N-1 DO
                        BEGIN
                            A1 ← A1 + PM[Q,I]
                            B1 ← B1 + PM[Q,I]*2
                        END
                    B1 ← B1/(N-1)
                    INT ← A1/(N-1)
                    POL ← SQRT (B1 - INT*2)
                    IF Q = 0
                        THEN
                            WRITE (FIL2[NO], FMT5, INT, POL)
                        ELSE
                            WRITE (FIL2[NO], FMT6, INT, POL)
                    IF LAMBDA < LMB1
                        THEN
                            Q ← 1
                            END
                L3:  WRITE (FIL2)
                    WRITE (FTP1, 9, TAPE[*])
                    GO TO L1
                L4:  END
                    GO TO L1
                L2:  REWIND (FTP1)
                    WHILE TRUE DO
                        BEGIN
                            READ (FTP1, 9, B[*])[L3]
                            WRITE (FPUNCH, FMT27, FOR I←0 STEP 1 UNTIL 8 DO B[I])
                        END
                L3:  CLOSE (FTP1, PURGE)
                    WRITE (FIL2, FMT7, TIME(2)/60, TIME(3)/60)
                    CLOSE (FTAPE, PURGE)
                END
            END
END .

```

```

COMMENT == CALIBRATION PROGRAM
BEGIN INTEGER M, SMP, U, SENS
      REAL RNTIM1, RNTIM2, RNTIM3, PI, PI2
      FILE FIL2 6 (2,15)
      FILE FILIN1 (2,10)
      FILE IN FLDT1 "MULF2" "FTP1" (1,550)
      FILE FIL4 2 (1,10, SAVE 10)
REAL PROCEDURE ARCCOS(X)      VALUE X; REAL X
BEGIN REAL T ; IF ABS(X)=1.0 THEN T+1.57079633*SIGN(X) ELSE
      T + ARCTAN(X/SQRT(1 - X*2))
      ARCCOS + 1.57079633 - T END ARCCOS
REAL PROCEDURE ATAN(A,B) ; VALUE A,B ; REAL A,B
BEGIN REAL T; IF B=0 THEN T+1.57079633*SIGN(A) ELSE IF B<0 THEN
      T + 3.14159266 +ARCTAN(A/B) ELSE T+ARCTAN(A/B)
      IF T<0 THEN T+T+6.28318554
      ATAN + T END
FORMAT IN : FMTI1(3I4),
      FMTI2(4I6/7F10.6),
      FMTI3(6I2,X8,9L5),
      FMTI4(10I6)
FORMAT OUT FMT1("DATA PROCESSOR TIME: ", F8.2, " SECONDS"),
      FMT2("INPUT - OUTPUT TIME: ", F8.2, " SECONDS"),
      FMT3("TUBE LAM      CI      RR      RP      DELTA
      "      ZETA      ETA")
STREAM PROCEDURE WORD(A,B)
BEGIN SI + A; DI+ B; SI + SI - 8; DS + 8 CHR      END
PROCEDURE DATE(FILEID)
      FILE FILEID
BEGIN ALPHA D; INTEGER I,DAY,YR ; LABEL L1; INTEGER ARRAY MO[1:12]
      FORMAT OUT FMT("RUN DATE ", 12,"/",12,"/",12)
      FILL MO[*] WITH 31,28,31,30,31,30,31,31,30,31,30,31
      D +TIME(0)
      YR + 10*D.[18:6] + D.[24:6]
      DAY + 100*D.[30:6] + 10*D.[36:6] + D.[42:6]
      IF DAY > (IF YR MOD 4 = 0 THEN 366 ELSE 365) THEN
            GO TO L1
      I +0

```

```

FOR I ← 1 + 1 WHILE DAY > 0 DO
    DAY ← DAY - MO[I]
    IF YR MOD 4 = 0 THEN IF I=2 THEN DAY ← DAY-1
    I ← I-1
    DAY ← DAY + MU[I]
    WRITE (FILEID, FMT, I, DAY, YR)
L1:END DATE
PROCEDURE DAYTIM(FILEID)
    FILE FILEID
BEGIN
    INTEGER I1, I2, I3, T
    FORMAT OUT FMT("RUN TIME ", I2, ":", I2, ":", I2)
    T ← TIME(1) DIV 60
    I1 ← T DIV 3600
    I2 ← (T - I1×3600) DIV 60
    I3 ← T - I1×3600 - I2×60
    WRITE (FILEID, FMT, I1, I2, I3)
END
PROCEDURE SORT(X,K)
    VALUE K
    INTEGER K
    ARRAY X[0]
BEGIN
    INTEGER I,J,L
    ARRAY F[0:K-1]
    FOR J ← K-1 STEP -1 UNTIL 0 DO
        F[J] ← X[0]
        FOR I ← 1 STEP 1 UNTIL K-1 DO
            IF X[I] > F[J] THEN
                F[J] ← X[I]
                L ← I
            X[L] ← 0
        FOR I ← 0 STEP 1 UNTIL K-1 DO
            X[I] ← F[I]
        END
    END
PROCEDURE COMPUTE(N,M,X,T,A,E,U,FILEID)
    VALUE N,M,T,U
    FILE FILEID
    INTEGER N,M,U

```

```

    ARRAY X[0:0], A[0]
    INTEGER ARRAY E[0]
    REAL T
BEGIN INTEGER I,J,P, K,L
    REAL T1, T2, S, D
    BOOLEAN ZZ
    LABEL L1, L2
    ARRAY Z[0:M-1,0:M]
    ARRAY B,C[0:N-1]
    LIST LIST1(S, T1, T2, P),
    LIST2(FOR I ← 0 STEP 1 UNTIL P-1 DO [X[M,I],B[I],C[I]])
    FORMAT OUT FMT1("STANDARD DEVIATION ",F10.5/X3,2(E12.5,X6),X2,I3),
        FMT2(3(3(F10.5,X3)))
    ZZ ← FALSE
    E[0] ← P ← N
    FOR I ← 1 STEP 1 UNTIL N DO
        E[I] ← I-1
L1: T1 ← T2 ← 0
    FOR I ← 0 STEP 1 UNTIL M-1 DO
    FOR J ← 0 STEP 1 UNTIL M DO
        Z[I,J] ← 0
        FOR K ← 0 STEP 1 UNTIL R-1 DO
            Z[I,J] ← Z[I,J] + X[I,K]*X[J,K]
    FOR K ← M STEP -1 UNTIL 0 DO
        D ← 0
        FOR I ← 1 STEP 1 UNTIL K DO
            IF ABS(Z[I-1,0]) > D
                L ← I-1
                D ← ABS(Z[L,0])
        IF L > 0
            FOR J ← 0 STEP 1 UNTIL K DO
                D ← Z[L,J]
                Z[L,J] ← Z[0,J]
                Z[0,J] ← D
            FOR I ← 0 STEP 1 UNTIL M-1 DO
                A[I] ← Z[I,0]
            FOR J ← 1 STEP 1 UNTIL K DO

```

```

    BEGIN

```

```

    END

```

```

    BEGIN

```

```

    THEN BEGIN

```

```

    END

```

```

    THEN BEGIN

```

```

    END

```

```

    BEGIN

```

```

        D ← Z[0,J]/A[0]
        FOR I ← 1 STEP 1 UNTIL M-1 DO
            Z[I-1,J-1] ← Z[I,J] - A[I]×D
            Z[M-1,J-1] ← D
        IF D = 1 THEN GO TO L2
        FOR I ← 0 STEP 1 UNTIL P-1 DO
            B[I] ← A[0]×X[0,I]
            FOR J ← 1 STEP 1 UNTIL M-1 DO
                B[I] ← B[I] + A[J]×X[J,I]
            C[I] ← X[M,I] - B[I]
            T1 ← T1 + C[I]
            T2 ← T2 + C[I]*2
        T1 ← T1/P
        T2 ← T2/P
        S ← SQRT(T2 - T1*2)
        IF U > 3 THEN WRITE (FILEID, FMT2, LIST2)
        WRITE (FILEID, FMT1, LIST1)
        IF U = 3 OR U = 5 THEN
            IF Z4 THEN GO TO L2
            ZZ ← TRUE
            P ← 0
            FOR I ← 0 STEP 1 UNTIL N-1 DO
                IF ABS(C[I]) < T×S
                    FOR J ← 0 STEP 1 UNTIL M DO
                        X[J,P] ← X[J,I]
                    E[P+1] ← I
                    P ← P + 1
            E[0] ← P
            GO TO L1
L2:END COMPUTE
REAL PROCEDURE CALCPM(T,X)
    VALUE T,X ; REAL X; INTEGER T
BEGIN INTEGER J ; REAL S1
    ARRAY I[0:72], V[0:1,0:72]
    FILL I[*] WITH 0,
    1.0e-4, 6.0e-4, 1.0e-3, 2.0e-3, 3.0e-3, 4.0e-3, 5.0e-3, 6.0e-3,
    7.0e-3, 8.0e-3, 9.0e-3, 1.0e-2, 1.1e-2, 1.2e-2, 1.3e-2, 1.4e-2,

```

```

1.5e-2, 1.6e-2, 1.7e-2, 1.8e-2, 1.9e-2, 2.0e-2, 2.2e-2, 2.4e-2,
2.6e-2, 2.8e-2, 3.0e-2, 3.5e-2, 4.0e-2, 4.5e-2, 5.0e-2, 5.5e-2,
6.0e-2, 7.5e-2, 8.0e-2, 8.5e-2, 9.0e-2, 9.5e-2, 1.0e-1, 1.5e-1,
2.0e-1, 2.5e-1, 3.0e-1, 3.5e-1, 4.0e-1, 4.5e-1, 5.0e-1, 5.5e-1,
6.0e-1, 6.5e-1, 7.0e-1, 7.5e-1, 8.0e-1, 8.5e-1, 9.0e-1, 9.5e-1,
1.0e-0, 1.1e-0, 1.2e-0, 1.3e-0, 1.4e-0, 1.5e-0, 1.6e-0, 1.7e-0,
1.8e-0, 1.9e-0, 2.0e-0, 2.1e-0, 2.2e-0, 2.3e-0, 2.4e-0, 2.5e-0 ;
FILL V[0,*] WITH 0.018,
0.040, 0.169, 0.270, 0.501, 0.769, 1.003, 1.240, 1.520,
1.710, 1.880, 2.010, 2.090, 2.130, 2.190, 2.225, 2.260,
2.296, 2.330, 2.351, 2.380, 2.400, 2.430, 2.460, 2.498,
2.520, 2.540, 2.560, 2.595, 2.630, 2.650, 2.690, 2.718,
2.740, 2.795, 2.802, 2.820, 2.850, 2.865, 2.880, 3.030,
3.100, 3.235, 3.280, 3.400, 3.465, 3.530, 3.570, 3.645,
3.690, 3.751, 3.810, 3.870, 3.930, 3.985, 4.040, 4.095,
4.150, 4.245, 4.350, 4.450, 4.550, 4.660, 4.750, 4.852,
4.951, 5.051, 5.179, 5.250, 5.340, 5.430, 5.470, 5.510 ;
FILL V[1,*] WITH 0.019,
0.038, 0.040, 0.245, 0.488, 0.750, 0.990, 1.210, 1.430,
1.630, 1.750, 1.860, 1.940, 1.995, 2.040, 2.070, 2.100,
2.128, 2.155, 2.180, 2.208, 2.230, 2.250, 2.296, 2.330,
2.360, 2.385, 2.400, 2.448, 2.480, 2.503, 2.540, 2.570,
2.595, 2.675, 2.690, 2.715, 2.738, 2.750, 2.765, 2.885,
2.980, 2.080, 3.165, 3.235, 3.288, 3.345, 3.370, 3.400,
3.500, 3.555, 3.610, 3.670, 3.720, 3.777, 3.845, 3.895,
3.920, 4.032, 4.128, 4.228, 4.318, 4.420, 4.500, 4.600,
4.695, 4.785, 4.880, 4.970, 5.058, 5.155, 5.249, 5.350 ;
IF T = 0 THEN S1 ← 0.7796 + 0.003196 × X ELSE S1 ← 0.9028 + 0.003254 × X ;
IF S1 < V[T,0] THEN S1 ← V[T,0] ELSE IF S1 > V[T,72] THEN S1 ← V[T,72] ;
J ← 0 ;
DO J ← J + 9 UNTIL S1 ≤ V[T,J] ;
DO J ← J - 1 UNTIL S1 ≥ V[T,J] ;
CALCPM ← (I[J] + (I[J+1] - I[J]) × (S1 - V[T,J]) / (V[T,J+1] - V[T,J])) END ;
PI ← 3.14159265 ;
PI2 ← PI/2 ;
SENS ← 0 ;
DATE (FIL2) ;

```



```

DAYTIM(FIL2)
WRITE (FIL2(100))
READ (FILIN1, FMT11, M, SMP, U)
BEGIN INTEGER Q, M1, L, STRTTM, LEVEL, LAMBDA1, LAMBDA2
REAL BKTIM, BRKTIM, OMGA, PSID
ARRAY PSI(0:M-1), ETAAR, ZETAAR(0:1)
INTEGER ARRAY N(0:M-1), OPT(0:5), LAMBDA(0:U-1)
FILE FTAPE1 2 (1, 3*SMP+4, SMP, SAVE 10)
BOOLEAN ARRAY Z(0:10)
ALPHA TUBE
LABEL L1
LIST LIST11(STRTTM, LEVEL, LAMBDA1, LAMBDA2, BRKTIM, OMGA, PSID,
ETAAR(0), ETAAR(1), ZETAAR(0), ZETAAR(1)),
LIST12(FOR L=0 STEP 1 UNTIL 5 DO OPT(L), FOR L=0 STEP 1
UNTIL 8 DO Z(L)),
LIST13(FOR L=0 STEP 1 UNTIL U-1 DO LAMBDA(L))
READ (FILIN1, FMT12, LIST11)
READ (FILIN1, FMT13, LIST12)
READ (FILIN1, FMT14, LIST13)
CLOSE (FILIN1, RELEASE)
FOR L=0 STEP 1 UNTIL M-1 DO
N(L) = SMP
PSI(L) = L*PSID*0.0174532925
SORT (LAMBDA, U)
WORD(FLDT1(0), M1)
BEGIN INTEGER I, J, K, P, R
REAL S, OMEGA, OMIN, OMAX, A1, B1
ALPHA ARRAY A(0:M1+5)
BOOLEAN Z1
ARRAY G(0:M1/4), GEN(0:SMP-1), H(0:1, 0:SMP-1), TIM(0:M-1), C(0:21)
INTEGER ARRAY BLOCK(0:M-1)
LABEL L1, L2, L3, L4, L5, L6, L7, LE1, LE2, LE3, LP1, LP2, LP3
LIST LIST1 (K, A1, B1, C(K), OMEGA),
LIST2(FOR I=0 STEP 1 UNTIL N(R)-1 DO GEN(I)),
LIST3(FOR I=0 STEP 1 UNTIL N(R)-1 DO H(0, I)),
LIST4(FOR I=0 STEP 1 UNTIL N(R)-1 DO H(1, I)),
LIST5(FOR I=0 STEP 1 UNTIL M-1 DO (BLOCK(I), TIME(I)))

```

```

FORMAT OUT FMT1("REFERENCE GENERATOR FREQUENCY APPROXIMATION"),
FMT2(10(F7.1,X4)),
FMT3("ARRAY GEN[*] = GENERATOR OUTPUT"),
FMT4("ARRAY H[0,*] = 30 KC PM TUBE"),
FMT5("ARRAY H[1,*] = 40 KC PM TUBE"),
FMT6("CALIBRATION TIMES AND BLOCK NUMBERS"),
FMT7(5(I5,X2,F10.3,X4)),
FMT8(I2, X2, 3(E15.0,X4),X3, F10.6),
FMT9("START TIME TOO LARGE"),
FMT10("END OF FILE -- R= ", I3),
FMT11("END OF FILE - STAGE 2 -- R= ", I3),
FMT12("PROGRAM ERROR - END OF FILE CALIBRATION TAPE"),
FMT13("PARITY ERROR BEFORE STARTING TIME -- BLOCK: ", I4),
FMT14("PARITY ERROR STAGE 1 - BLOCK: ", I4,X3,"R= ", I3),
FMT15("PARITY ERROR STAGE 2 - BLOCK: ", I4,X3,"R= ", I3),
FMT16(///"# ", I2," RELATIVE ANGLE OF INCIDENT POLARIZATION",
      " -- ", F8.3, " RADIANS"),
FMT17(// "NUMBER OF SAMPLES PER ANGLE OF INCIDENT",
      " POLARIZATION: ", I4/"NUMBER OF ANGLES OF INCIDENT",
      " POLARIZATION: ", I3)
;

L ← 0
;
R ← -1
;
P ← (M1-3) DIV 4 + 1
;
L1: READ (FLDT1,2,A[*])(LE1:LP1)
;
IF A[1].[30:17] < STRTTM THEN
;
GO TO L1
;
SPACE (FLDT1,-1)[L5]
;
L2: READ (FLDT1[N0], 1, A[*])(LE2:LP2)
;
WORD (FLDT1(0), M1)
;
READ (FLDT1, M1, A[*])
;
IF Z1 AND A[M1-1].[1:13] < LAMBDA[L] THEN
;
GO TO L2
;
FOR J ← 3 STEP 4 UNTIL M1-1 DO BEGIN
;
IF A[J+1].[14:11] > LEVEL THEN
;
IF NOT Z1 THEN BEGIN
;
R ← R+1
;
Z1 ← TRUE
;
END
;

```

```

IF Z1 THEN
IF A[J].[1:13] = LAMBDA[L] THEN BEGIN
    TIM[R] ← A[I].[30:17] + A[J].[25:8] - A[3].[25:8]
    + A[J].[39:10]/1000 ;
    BLOCK[R] ← A[0] ;
    IF R=0 AND L=0 THEN
        FOR I ← 0 STEP 1 UNTIL R DO
            G[I] ← A[4×I+3].[14:11] ;
        K ← J-2 ;
        FOR I ← 0 STEP 1 UNTIL N[R]-1 DO BEGIN
            IF 4×I+K > M1-2 THEN BEGIN
                READ (FLDT1, M1, A[*])[LE3:LP3] ;
                SPACE(FLDT1,-1) ;
                K ← 5 - 4×I ;
                IF A[4×I+K].[43:5] ≠ 3 THEN END ;
                K ← K + 1 ;
                GO TO L3 ;
                GEN[I] ← A[4×I+K-2].[14:11] ;
                H[0,I] ← A[4×I+K].[14:11] ;
                H[1,I] ← A[4×I+K+1].[14:11] ;
            END ;
        END BEGIN
    IF Z10] THEN BEGIN
        WRITE (FIL2, FMT16, R, HSI[R]) ;
        WRITE (FIL2, FMT3) ;
        WRITE (FIL2, FMT2, LIST2) ;
        WRITE (FIL2, FMT4) ;
        WRITE (FIL2, FMT2, LIST3) ;
        WRITE (FIL2, FMT5) ;
        WRITE (FIL2, FMT2, LIST4) ;
        WRITE (FTAPE1, N[R], GEN[*]) ;
        WRITE (FTAPE1, N[R], H[0,*]) ;
        WRITE (FTAPE1, N[R], H[1,*]) ;
        SPACE (FLDT1,-1) ;
        L ← L + 1 ;
        IF L < U THEN
            GO TO L2
            Z1 ← FALSE
        ELSE BEGIN

```

```

                IF R < M-1
                    L ← 0
                    GO TO L2
                GO TO L4

    GO TO L2
LE1:  WRITE (FIL2, FMT9)
      SENS ← 1
      GO TO L4
LE2:  WRITE (FIL2, FMT10, R)
      IF R > 6
          M ← R + 1
          SENS ← 1
      GO TO L4
LE3:  WRITE (FIL2, FMT11, R)
      IF R > 7
          M ← R
          SENS ← 1
      GO TO L4
LE5:  WRITE (FIL2, FMT12)
      SENS ← 1
      GO TO L4
LP1:  RELEASE (FLDT1)
      WRITE (FIL2, FMT13, A[0])
      GO TO L1
LP2:  RELEASE (FLDT1)
      WRITE (FIL2, FMT14, A[0], R)
      Z1 ← FALSE
      FOR I ← R STEP 1 UNTIL M-2 DO
          PSI[I] ← PSI[I+1]
      M ← M-1
      IF M > 8
          SENS ← 1
          GO TO L4
      IF R < M
          GO TO L2

```

```

    THEN BEGIN
        ;
    END
ELSE
    END
    END END
    ;
    ;
    ;
    ;
    THEN
ELSE
    ;
    ;
    ;
    THEN
ELSE
    ;
    ;
    ;
    ;
    ;
    ;
    ;
    ;
    ;
    THEN BEGIN
        ;
    END
    ;
    THEN
ELSE

```

	GO TO L4		;
LP3:	RELEASE (FLDT1)		;
	WRITE (FIL2, FMT15, A[0], R)		;
	Z1 ← FALSE		;
	FOR I ← R STEP 1 UNTIL M-2 DO		
	PSI[I] ← PSI[I+1]		;
	M ← M-1		;
	IF M > 8	THEN BEGIN	;
	SENS ← 1		;
	GO TO L4	END	;
	IF R < M	THEN	
	GO TO L2	ELSE	
	GO TO L4		;
L4:	REWIND (FTAPE1)		;
	IF ZL1]	THEN BEGIN	;
	WRITE (FIL2, FMT17, SMP, M)		;
	WRITE (FIL2, FMT6)		;
	WRITE (FIL2, FMT7, LIST5)	END	;
	LOCK (FLDT1, RELEASE)		;
	OMIN ← 0.9×OMGA		;
	OMAX ← 1.1×OMGA		;
	S ← (OMAX-OMIN)/10.0		;
	IF ZL2]	THEN	
	WRITE (FIL2, FMT1)		;
L6:	K ← 0		;
	FOR OMEGA ← OMIN STEP S UNTIL OMAX DO	BEGIN	;
	A1 ← B1 ← 0		;
	FOR I ← 0 STEP 1 UNTIL R DO	BEGIN	;
	A1 ← A1 + G[I]×COS(I×OMEGA)		;
	B1 ← B1 + G[I]×SIN(I×OMEGA)	END	;
	C[K] ← A1*2 + B1*2		;
	IF ZL2]	THEN	
	WRITE(FIL2, FMT8, LIST1)		;
	K ← K + 1	END	;
	A1 ← C[0]		;
	FOR I ← 1 STEP 1 UNTIL M-1 DO		
	IF C[I] > A1	THEN BEGIN	

```

                A1 ← C[I]
                OMGA ← OMIN + I×S
            IF (OMAX-UMIN)/OMGA < 0.01
            THEN
                GO TO L7
            UMIN ← OMGA - S
            OMAX ← OMGA + S
            S ← S/10.0
            GO TO L6
L7:END *
        IF SENS = 1
        THEN
            GO TO L1
        FOR L ← 0 STEP 1 UNTIL U-1 DO
BEGIN INTEGER I, J, Q, K
    ARRAY GEN[0:SMP-1], PM[0:1, 0:M-1, 0:SMP-1], A[0:7],
        X[0:7, 0:IF M>SMP THEN M-1 ELSE SMP-1], THETA2[0:M-1, 0:SMP-1];
    REAL PHI, AMP, R, OMEGA
    INTEGER ARRAY BE[0:SMP]
    LIST LIST1(FOR I ← 0 STEP 1 UNTIL N[J]-1 DO THETA2[J, I])
    FORMAT OUT FMT1(/"REFERENCE GENERATOR DATA -- SMALL ANGLE APPROXIMATION"
        ),
        FMT2(9(F10.5, X2)),
        FMT3(/"REFERENCE GENERATOR CURVEFITTING DATA"),
        FMT4(3(F12.6, X4)/X2, 3(F12.6, X2))
    SPACE (FTAPE1, 3×L)
    FOR J ← 0 STEP 1 UNTIL M-1 DO
        BEGIN
            READ (FTAPE1, N[J], GEN[*])
            READ (FTAPE1, N[J], PM[0, J, *])
            READ (FTAPE1, N[J], PM[1, J, *])
            IF J ≠ M-1
            THEN
                SPACE(FTAPE1, 3×(U-1))
            FOR I ← 0 STEP 1 UNTIL SMP-1 DO
                BEGIN
                    X[0, I] ← 1.0
                    X[1, I] ← SIN(I×OMGA)
                    X[2, I] ← COS(I×OMGA)
                    FOR K ← 1, 2 DO
                        BEGIN
                            X[2×K+1, I] ← X[1, I]×(I×K)
                            X[2×K+2, I] ← X[2, I]×(I×K)

```

```

        X[7,I] ← GEN[I]                                END ;
    COMPUTE (N[J],7,X,1.2,A,B,OPT[0],FIL2)             ;
    PHI ← ATAN(A[2],A[1])                               ;
    IF ABS(A[4]-A[3]) > 0.001 THEN                     ;
        IF ABS(A[2]) > ABS(A[1]) THEN                 ;
            OMGA ← OMGA - A[3]/A[2]                   ELSE ;
            OMGA ← OMGA + A[4]/A[1]                     ;
    IF ZL3] THEN BEGIN ;
        WRITE (FIL2, FMT1) ;
        WRITE (FIL2, FMT2, PHI,OMGA,FOR I←0,1,2,3,4,5,6 DO A[I])END ;
    FOR I ← 0 STEP 1 UNTIL B[0]-1 DO BEGIN ;
        X[1,I] ← SIN(OMGA×B[I+1]) ;
        X[2,I] ← COS(OMGA×B[I+1]) ;
        X[3,I] ← GEN[B[I+1]] END ;
    COMPUTE (B[0],3,X,1.2,A,B,OPT[1],FIL2)             ;
    PHI ← ATAN(A[2],A[1])                               ;
    AMP ← SQRT(A[1]*2+A[2]*2)                           ;
    IF ZL4] THEN BEGIN ;
        WRITE (FIL2, FMT3) ;
        WRITE (FIL2, FMT4,A[0],AMP,PHI,FOR I←0,1,2 DO A[I]) END ;
    FOR I ← 0 STEP 1 UNTIL N[J]-1 DO BEGIN ;
        R ← (GEN[I]-A[0])/AMP ;
        OMEGA ← PHI + I×OMGA ;
        IF I > 1 THEN ;
            OMEGA ← (2×THETA2[J,I-1]-THETA2[J,I-2]+OMEGA)/2 ;
        IF ABS(R) ≤ 1.0 THEN BEGIN ;
            R ← PI/2 - ARCCOS(R) ;
            K ← ENTIER(OMEGA/PI/2) ;
            IF K ≤ 0 THEN ;
                THETA2[J,I] ← R ELSE BEGIN ;
                    K ← K+1 ;
                    IF K MOD 4 ≤ 1 THEN ;
                        THETA2[J,I] ← PI×(K DIV 2) + R ;
                    ELSE ;
                        THETA2[J,I] ← PI×(K DIV 2) - R ;
            END ;
        END ;
    END ;
END
END

```



```

LIST10(Q,LAMBDA[L], CI, RR, RP, DELTA, ZETA, ETA),
LIST11(POL,V,PHI)
FORMAT OUT FMT1("/ARRAY B"),
FMT2(5(E12.5, X4)),
FMT3("/ARRAY C"),
FMT4("ETA ", F9.6, X4, "X12 ", 2(F8.6, X3)/"ZETA", F9.6/),
FMT5("/ARRAY A"),
FMT6("/ARRAY D"),
FMT7("/COMPUTE ERROR = ARRAY D"/5(I2, X1, E12.5, X3)/
4(I2, X1, E12.5, X3)/I2, X1, E12.5, X3),
FMT8("/COMPUTE ERROR = ARRAY D"/2(5(I2, X1, E12.5, X3)/),
"RR2= ", E12.5/"RP2= ", E12.5),
FMT9("/COMPUTE ERROR = ARRAY D"/2(5(I2, X1, E12.5, X3)/),
"RR= ", F10.5/"COS(DELTA)= ", E12.5/"RP2= ", E12.5),
FMT10("/COMPUTE ERROR = ARRAY D"/2(5(I2, X1, E12.5, X3)/),
"RR= ", F10.5/"DELTA= ", F10.6/"RP2= ", E12.5),
FMT11(X4, A4),
FMT12("LAMBDA: ", I5/"CI ", E13.6, X3, "RR ", F10.8, X3, "RP ",
F10.8, X3, "DELTA ", F12.8/X19, "ZETA ", F10.7, X1, "ETA ",
F10.7),
FMT13(I2, X2, I4, X2, E13.6, 5(F10.7, X1)),
FMT14(X63, "P ", F6.3, X4, "V ", F6.3, "PHI", F7.3)
FOR I ← 0 STEP 1 UNTIL IF SMP>M THEN SMP-1 ELSE M-1 DO
X[0, I] ← 1.0
IF Z[L+Q] THEN BEGIN
ETA ← ETAAR[Q]
ZETA ← ZETAAR[Q]
U1[0] ← SMP
FOR I ← 0 STEP 1 UNTIL SMP-1 DO
U1[I+1] ← I
FOR I ← 0, 1, 2, 3, 4 DO BEGIN
U2[I, 0] ← M
FOR J ← 0 STEP 1 UNTIL M-1 DO
U2[I, J+1] ← J
END
GO TO L1
END
FOR J ← 0 STEP 1 UNTIL M-1 DO BEGIN
FOR I ← 0 STEP 1 UNTIL N[J]-1 DO BEGIN

```

```

        X[1,I] ← SIN(THETA2[J,I])
        X[2,I] ← COS(THETA2[J,I])
        X[3,I] ← SIN(2*THETA2[J,I])
        X[4,I] ← COS(2*THETA2[J,I])
        X[5,I] ← PM[Q,J,I]
        COMPUTE (NIJ,5,X,0.9,B[J,*], U1,OPT[2],FIL2)
WRITE (FIL2, FMT1)
WRITE (FIL2, FMT2, LIST1)
FOR J ← 0 STEP 1 UNTIL M-1 DO
    PSI2 ← 2*PSI[J]
    X[1,J] ← X1[0,J] ← SIN(PSI2)
    X[2,J] ← X1[1,J] ← COS(PSI2)
FOR I ← 0,1,2 DO
    FOR J ← 0 STEP 1 UNTIL M-1 DO
        X[3,J] ← B[J,I]
        COMPUTE (M,3,X,0.9,C[I,*],U2[I,*],ORT[3],FIL2)
FOR I ← 3,4 DO
    FOR J ← 0 STEP 1 UNTIL M-1 DO
        X[0,J] ← X1[0,J]
        X[1,J] ← X1[1,J]
        X[2,J] ← B[J,I]
        COMPUTE (M,2,X,0.9,C[I,*],U2[I,*],OPT[3],FIL2)
WRITE (FIL2, FMT3)
WRITE (FIL2, FMT2, LIST2)
ETA ← 0.5*ATAN(-C[0,1],C[0,2])
XI21 ← 0.5*ATAN(C[3,1],C[3,0])
XI22 ← 0.5*ATAN(-C[4,0],C[4,1])
IF ABS(XI21-XI22) < 0.26
    ZETA ← (ETA + (XI21+XI22)/2)/2
    IF ABS(C[3,1]) > ABS(C[4,2])
        ZETA ← (ETA - XI21)/2
        ZETA ← (ETA - XI22)/2
WRITE (FIL2, FMT4, LIST3)
FOR I ← 0 STEP 1 UNTIL IF SMR>M THEN SMP-1 ELSE M-1 DO
    X[0,I] ← 1.0
L1: FOR J ← 0 STEP 1 UNTIL M-1 DO
    FOR I ← 0 STEP 1 UNTIL M1[0]-1 DO

```

END

END

BEGIN

END

BEGIN

END

BEGIN

BEGIN

END

END

THEN

ELSE

THEN

ELSE

```

        BETA2 ← ZETA×2 + TETA2[J,U1[I+1]]
        X[1,I] ← SIN(BETA2)
        X[2,I] ← COS(BETA2)
        X[3,I] ← SIN(2×BETA2)
        X[4,I] ← COS(2×BETA2)
        X[5,I] ← PM[Q,J,U1[I+1]]
        COMPUTE(U1[0],5,X,0.9,A1[J,*],U3,DPT[4],FIL2)
WRITE (FIL2,FMT5)
WRITE (FIL2,FMT2,LIST4)
FOR I ← 0 STEP 1 UNTIL M-1 DO
    X1[0,I] ← SIN(2×(PSI[I] + ETA))
    X1[1,I] ← COS(2×(PSI[I] + ETA))
    FOR I ← 0,1,2 DO
        FOR J ← 0 STEP 1 UNTIL U2[I,0]-1 DO
            X[1,J] ← X1[IF I=1 THEN 0 ELSE 1,U2[I,J+1]]
            X[2,J] ← A1[U2[I,J+1],I]
            COMPUTE (U2[I,0],2,X,0.9,A,U4[I,*],OPT[5],FIL2)
            FOR J ← 0,1 DO
                D[2×I+J] ← A[J]
            FOR I ← 3,4 DO
                FOR J ← 0 STEP 1 UNTIL U2[I,0]-1 DO
                    X[0,J] ← X1[IF I=4 THEN 1 ELSE 0,U2[I,J+1]]
                    X[1,J] ← A1[U2[I,J+1],I]
                    COMPUTE (U2[I,0],1,X,0.9,A,U4[I,*],OPT[5],FIL2)
                    D[2×I] ← A[0]
                WRITE (FIL2,FMT6)
                WRITE (FIL2,FMT2,LIST5)
                FOR I ← 0 STEP 1 UNTIL 9 DO
                    D[I] ← ABS(D[I])
                    D[3] ← (D[3] + D[5])/2
                    D[5] ← (D[6] + D[8])/2
                    D[6] ← (D[0] - D[4])/(D[0] + D[4])
                    D[7] ← (D[1] + D[5] - D[8])/(D[1] + D[5] + D[3])
                    D[8] ← D[6]×D[7]
                    D[9] ← (1 - D[6]×2)×(1 - D[7]×2)
                IF D[9] ≥ 0
                    D[9] ← SQRT(D[9])

```

END ;

END ;

BEGIN ;

END ;

BEGIN ;

BEGIN ;

END ;

END ;

BEGIN ;

BEGIN ;

END ;

END ;

;

;

;

;

;

;

;

;

;

;

THEN

ELSE

BEGIN

```

        WRITE (FIL2, FMT7, LIST5)
        GO TO L2
WRITE (FIL2, FMT6)
WRITE (FIL2, FMT2, LIST5)
RP2 ← (1 - D[8] - D[9]) / (D[6] - D[7])
RR2 ← (1 + D[8] - D[9]) / (D[6] + D[7])
IF RR2 ≥ 0
    THEN
        RR ← SQRT(RR2)
        WRITE (FIL2, FMT8, LIST6)
        GO TO L2
    ELSE
        BEGIN
        END
COSDLT ← ((D[1] - D[5]) / (D[1] + D[5])) × (1 + RR2) / (2 × RR)
IF ABS(COSDLT) ≤ 1.0
    THEN
        DELTA ← ARCCOS(COSDLT)
        WRITE (FIL2, FMT9, LIST7)
        GO TO L2
    ELSE
        BEGIN
        END
IF RP2 ≥ 0
    THEN
        RP ← SQRT(RP2)
        WRITE (FIL2, FMT10, LIST8)
        GO TO L2
    ELSE
        BEGIN
        END
CI ← D[0] / ((1 + RR2) × (1 + RP2))
WRITE (FIL2, FMT11, TUBE)
WRITE (FIL2, FMT12, LIST9)
IF Z[5]
    THEN
        WRITE (FIL4, FMT13, LIST10)
        FOR J ← 0 STEP 1 UNTIL M-1 DO
            PHI ← ATAN(A1[J,3], A1[J,4])
            IF PHI < 0
                THEN
                    PHI ← PHI + 6.28318534
            POL ← 2 × SQRT(A1[J,3]² + A1[J,4]²) / (CI × (1 - RP2) × (1 + RR2 - 2 × RR ×
                COSDLT))
            V ← (A1[J,1] × CI × (1 + RP2) × (1 - RR2) × POL × SIN(PHI)) / (2 × CI × RR ×
                (1 - RP2) × SIN(DELTA))
        PHI ← 0.5 × PHI
        WRITE (FIL2, FMT14, LIST11)
L2:END
IF LAMBDA[1] < LAMBDA1
    THEN
        Q ← 1

```

END		END	;
	IF Z15]	THEN	BEGIN
	REWIND (FIL4)		;
	IF Z16]	THEN	BEGIN
	WRITE (FIL2[PAGE])		;
	DATE (FIL2)		;
	DAYTIM (FIL2)		;
	WRITE (FIL2[DBL], FMT3)	END	;
BEGIN	LABEL L1,L2		;
	FILE FIL6 0 (3,10)		;
	ARRAY A[0:9]		;
	DATE (FIL6)		;
	DAYTIM (FIL6)		;
	WRITE (FIL6, FMT3)		;
L1:	READ (FIL4, 10, A[*])[L2]		;
	WRITE (FIL6, 10, A[*])		;
	IF Z16]	THEN	;
	WRITE (FIL2, 10, A[*])		;
	GO TO L1		;
L2:	IF Z16]	THEN	;
	WRITE (FIL2[PAGE])		;
	CLOSE (FIL4, PURGE)		;
END			;
		END	;
L1:END			;
	RNTIM2 ← TIME(2)/60		;
	WRITE (FIL2, FMT1, RNTIM2)		;
	RNTIM3 ← TIME(3)/60		;
	WRITE (FIL2, FMT2, RNTIM3)		;
END .			

BIBLIOGRAPHY

1. W. G. Fastie and G. H. Dieke, Final Report, Contract AF19(604)-5516, AFCRL 1060 (31 July 1961)
2. W. G. Fastie, Journal of the Optical Society of America, 42, 9, 641-647 (Sept. 1952)
3. Z. Sekera, Final Report, Contract AF19(122)-239, Dept. of Meteorology, University of California (1955)
4. C. R. N. Rao and Z. Sekera, Scientific Report No. 1, Contract AF19(604)-8050, AFCRL 63 809 (June 1963)
5. Z. Sekera, C. R. N. Rao and D. Dribble, Review of Scientific Instruments, 35, 764 (1963)
6. E. B. Hodgdon and H. D. Edwards, Final Report, Contract AF19(628)-2416, AFCRL 66 397 (April 1966)
7. R. Stain, W. E. Schneider and J. K. Jackson, Applied Optics, 2, 1151 (1963)
8. P. Bener, Tech. Note 2, Contract AF61(052)-618, AFCRL 63 654, Davos-Plate, Switzerland (Jan. 1963)
9. C. G. Stokes, Transactions of the Cambridge Philosophical Society, 2, 399 (1852)
10. H. Mueller, Journal of the Optical Society of America, 38, 661 (1948)